

TECHNICAL MEMORANDUM

To: Mr. Keith Van Der Maaten
General Manager, Marina Coast Water District

From: Curtis J. Hopkins
Principal Hydrogeologist, Hopkins Groundwater Consultants, Inc.

Date: May 26, 2016

Subject: North Marina Area Groundwater Data and Conditions

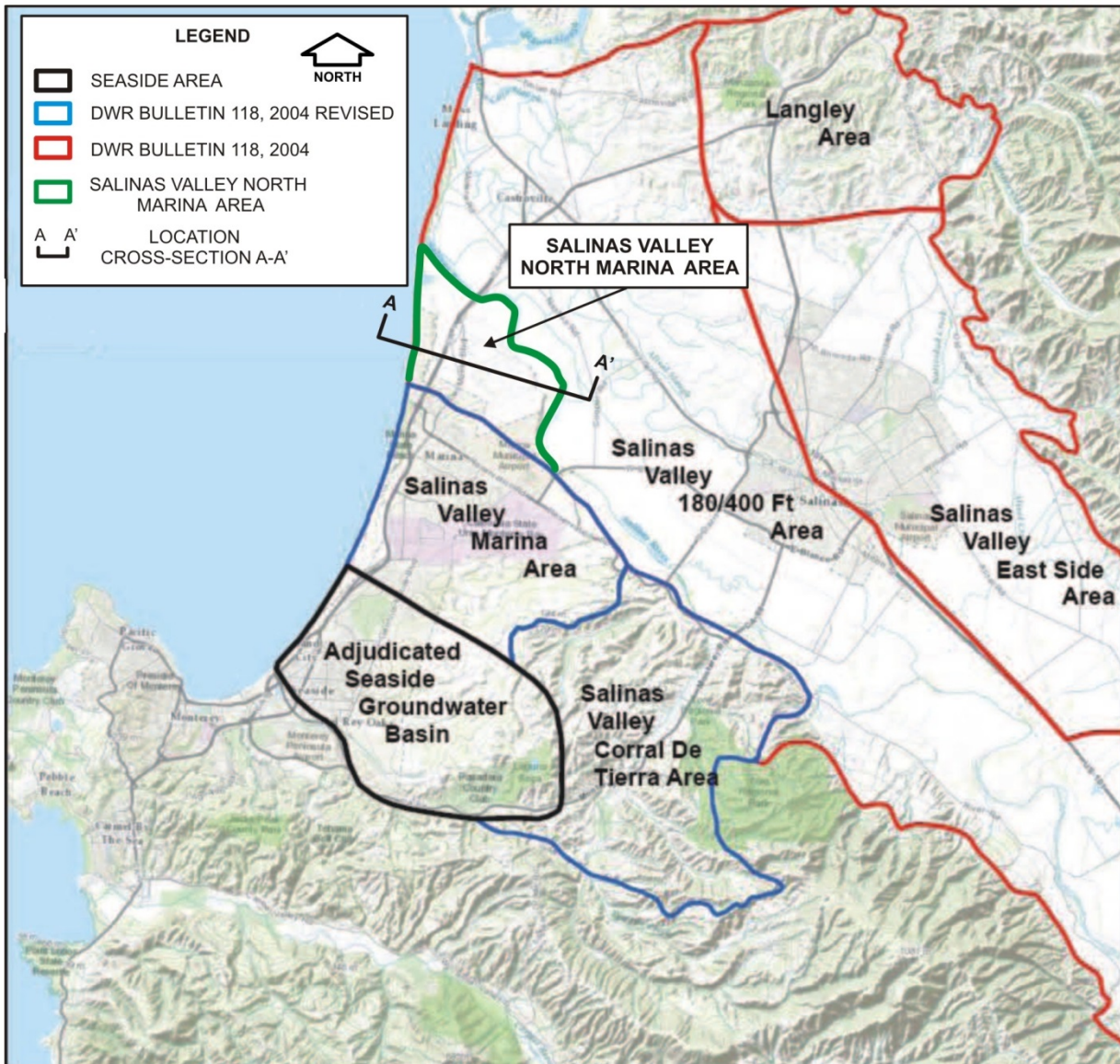
I. Introduction

Hopkins Groundwater Consultants, Inc. (Hopkins) has reviewed groundwater data provided by the California-American Water Company's (Cal-Am's) test slant well project for the Monterey Peninsula Water Supply Project (MPWSP) as requested by Marina Coast Water District (MCWD). This memorandum provides a summary of groundwater data and the conditions that are inferred from these data in the North Marina Area of the 180-400 Foot Aquifer Subbasin¹ within the Salinas Valley Groundwater Basin (SVGB). The North Marina Area is delineated for reference in Figure 1 – Groundwater Basin Boundary Map which shows its location within the SVGB. As shown, the North Marina Area is located between the northern boundary of the Marina Area and the Salinas River. This area of the basin has been largely undeveloped and historically contained very few wells to provide groundwater data.

The geology in the North Marina Area differs from the geology north of the Salinas River in the main portion of the 180-400 Foot Aquifer Subbasin and has been described in detail by studies conducted for the MPWSP. An interpretation of subsurface deposits within this specific coastal area is provided in Plate 1 – Cross-Section A-A', which is a portion of a subsurface profile constructed by Geoscience Support Services, Inc. from borehole data collected in the area (Geoscience, 2014). The approximate location of Cross-Section A-A' is shown in Figure 1. As shown and as described by previous study (Geoscience, 2014 and 2015, KJC, 2004), the terrace deposits that comprise the 180-Foot Equivalent Aquifer (180-FTE) in the North Marina Area grade into the alluvial deposits that comprise the 180-Foot Aquifer in the main portion of the basin around the present location of the Salinas River.

¹ / For purposes of the memorandum, the North Marina Area is defined as that portion of the 180/400 Foot Aquifer Subbasin located south of the Salinas River and north of the Salinas Valley Marina Area.

Figure 1 – Groundwater Basin Boundary Map

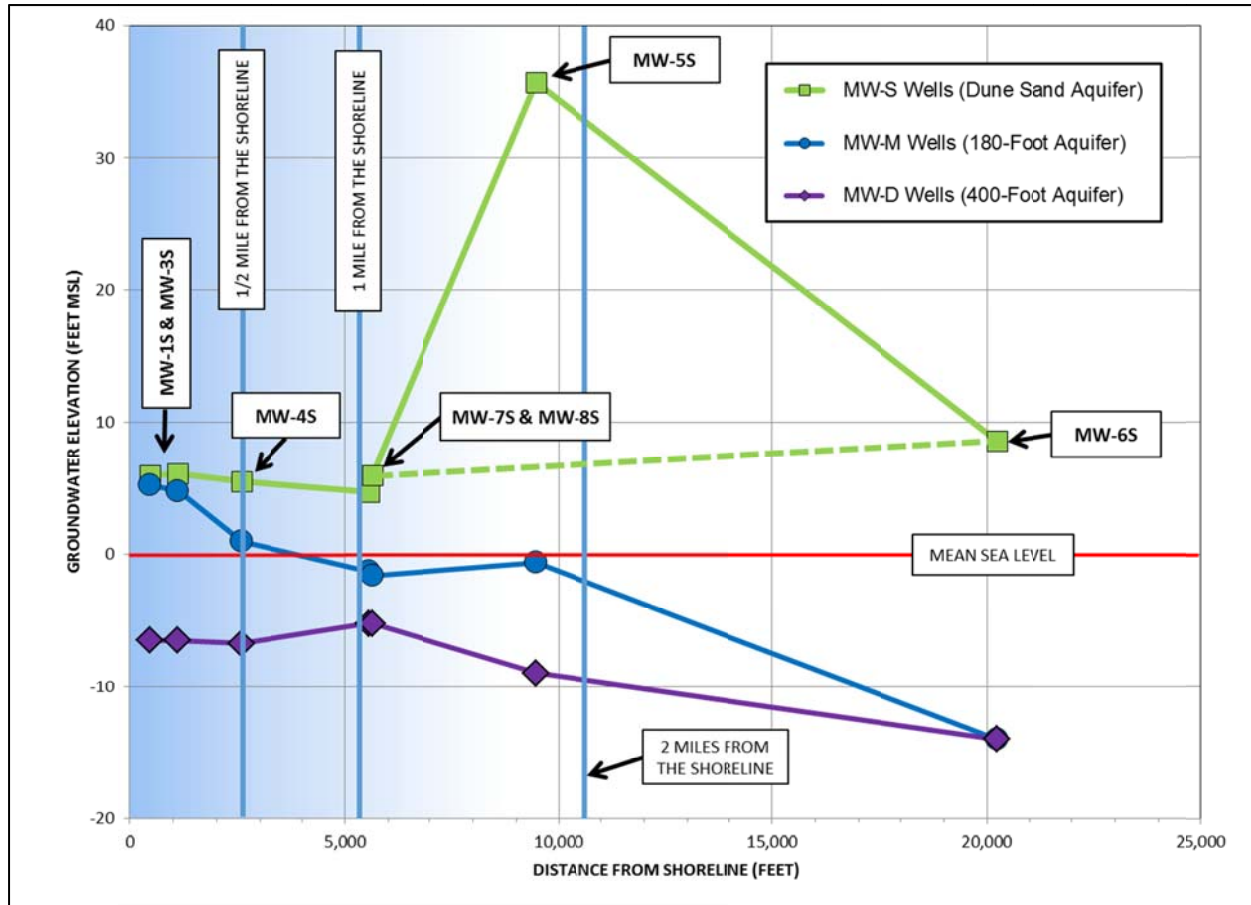


II. Coastal Groundwater Elevations

Recent investigation for the MPWSP includes the installation of a test slant well and multiple monitoring wells in and around the CEMEX property where the MPWSP intake wells are proposed to be located. The monitoring well network is being used to generate background water level and water quality data within the North Marina Area of the 180-400 Foot Aquifer Subbasin. The location of the monitoring facilities is shown on Plate 2 – Well Location Map. The construction details of these wells are included for reference as Attachment A – Well Construction Information.

Routine monitoring of the well network is presented in weekly summary reports that are posted on the Cal-Am website. Water level data are graphically presented as hydrographs which show daily changes and seasonal trends. A set of hydrographs provided by the MPWSP test slant well long term pumping test Monitoring Report No. 55 are included as Attachment B – MPWSP Water Level Data. We must note that while we have over a year of data, the climatic conditions prior to initiation of testing have been extremely dry. For comparison of the groundwater conditions across the area prior to resumption of pumping, data from May 2, 2016 were used to construct Figure 2 – Groundwater Elevation From MPWSP Monitoring Wells. As shown, the water level elevations vary significantly between the shallow Dune Sand Aquifer (indicated by the MW-S Wells), the 180-FTE Aquifer (indicated by the MW-M Wells), and the 400-Foot Aquifer (indicated by the MW-D Wells).

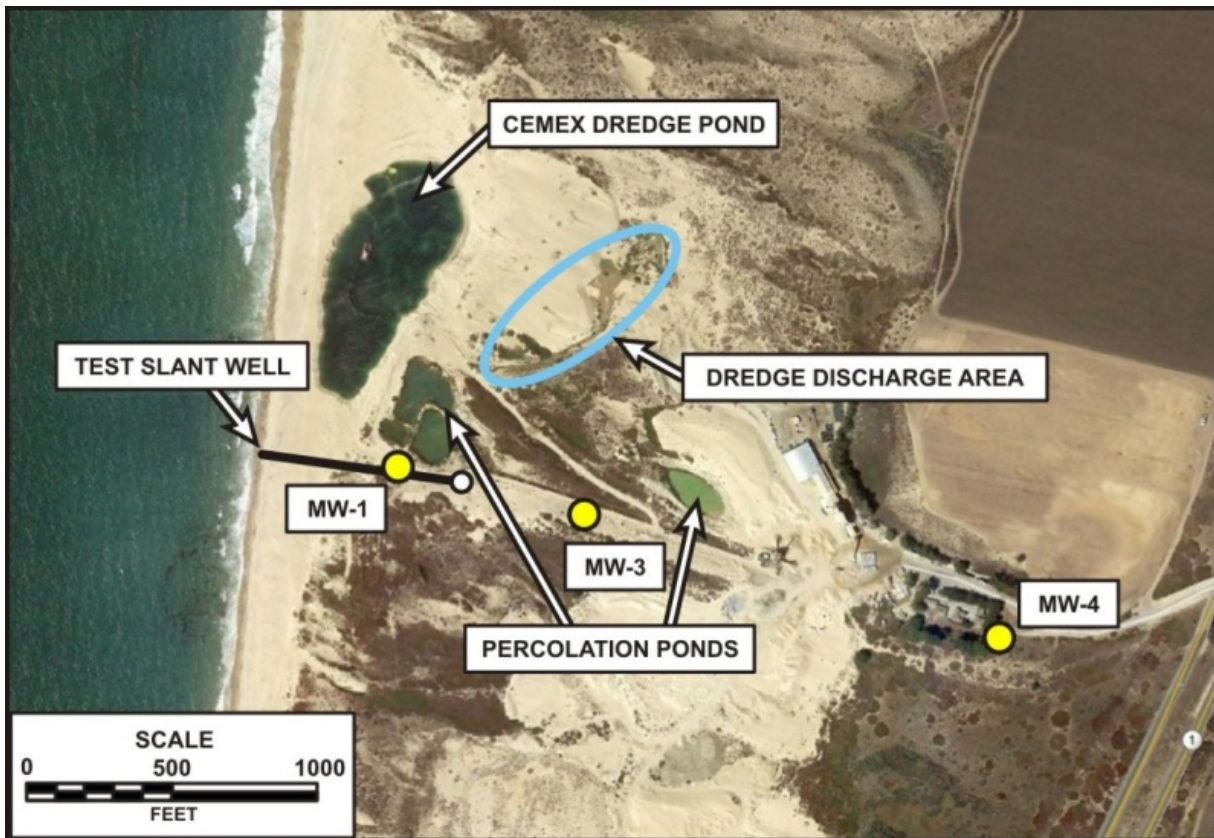
Figure 2 – Groundwater Elevation From MPWSP Monitoring Wells



The Dune Sand Aquifer has water levels that are notably above sea level and maintain a protective head against seawater intrusion (Geoscience, 2013). The coastal groundwater mounding at MW-1 and MW-3 is believed to be maintained by the CEMEX dredge pond operation that is discharged on the landward side of the coastal dunes as well as process water

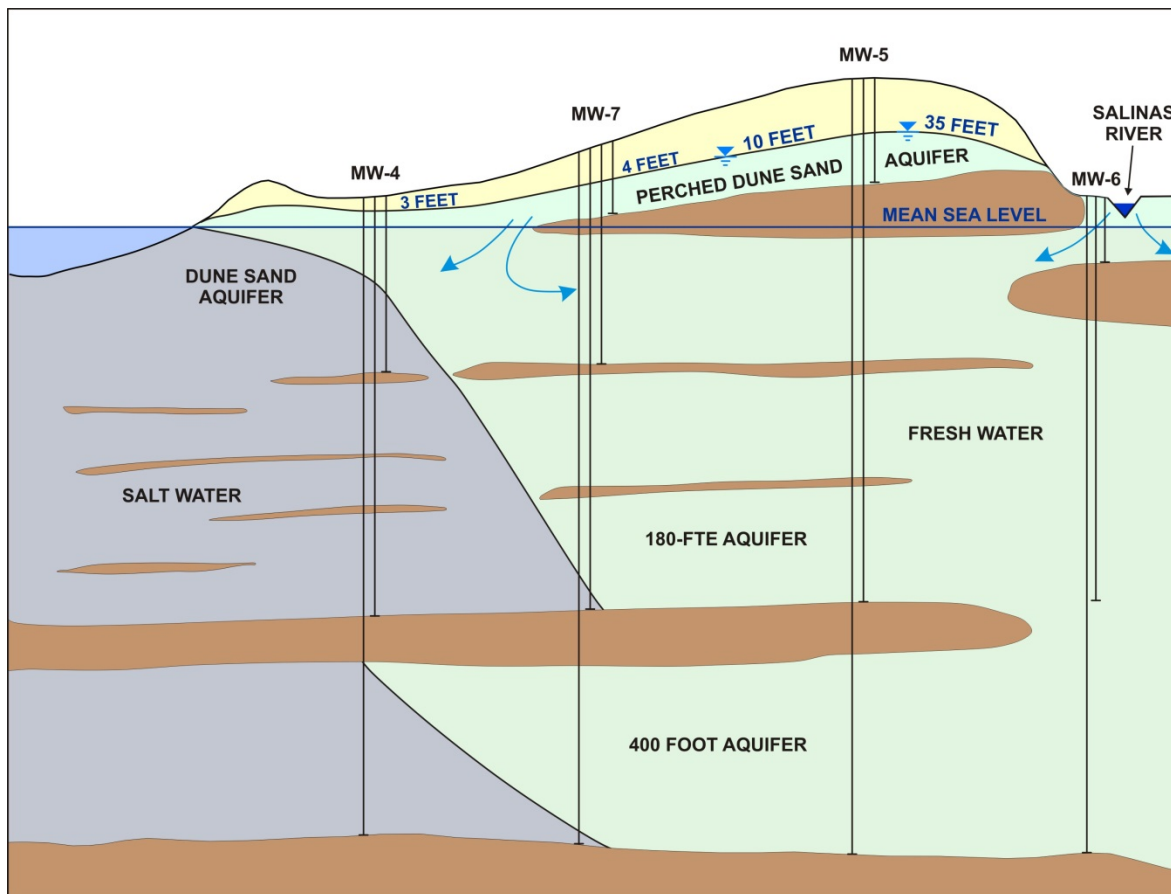
that is discharged to percolation ponds. Figure 3 – CEMEX Salt Water Discharge Locations shows the surface water features that have influenced the groundwater levels and quality at this location along the coast for decades. The maintenance of these features undoubtedly increases the amount of ocean water present in the vicinity of the test slant well.

Figure 3 – CEMEX Salt Water Discharge Locations



These data also show the perched groundwater condition in the vicinity of MW-5 where the groundwater elevation is 36 feet above mean sea level (msl). The groundwater perched above the Salinas Valley Aquitard equivalent flows toward the coast and results in downward recharge where the aquitard layer thins (or ends) and provides fresh water recharge into the coastal unconfined Dune Sand Aquifer and the underlying 180-Foot Aquifer in the vicinity of MW-7 and MW-8. Figure 4 – Conceptual Drawing of the Hydrogeology in the North Marina Area illustrates the subsurface conditions indicated by these available data.

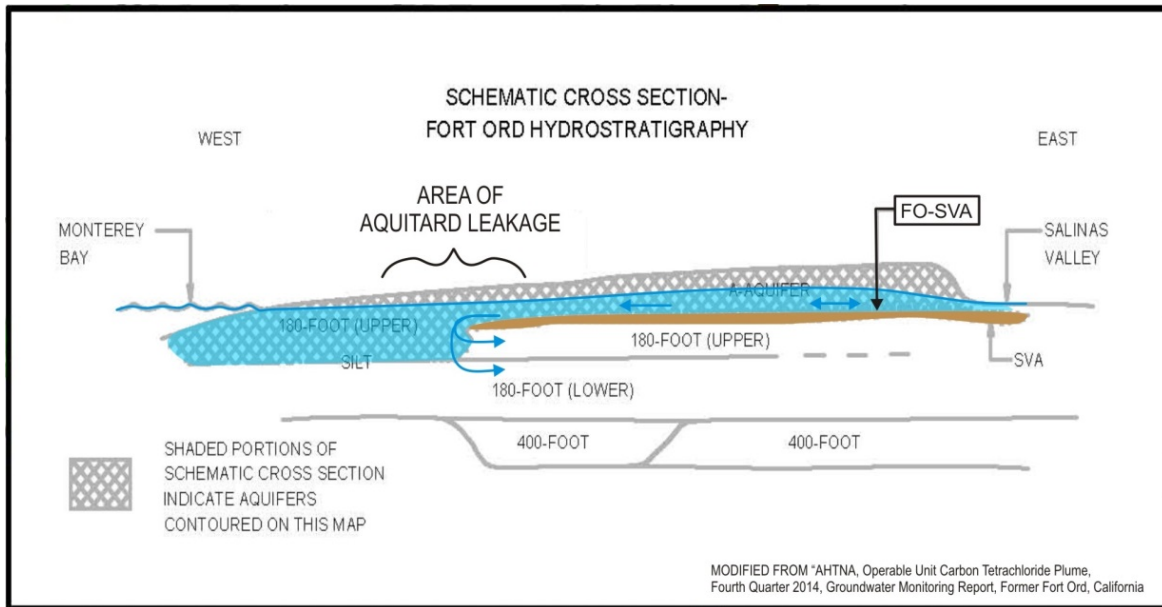
Figure 4 – Conceptual Drawing of the Hydrogeology in the North Marina Area



Years of reduced pumping has resulted in beneficial groundwater conditions that are apparently slowing the movement of seawater and providing a freshwater source that is replenishing the aquifers. Notably, the fact that the Dune Sand and 180-Foot Aquifers at Monitoring Well MW-7 are no longer contaminated by high concentrations of seawater can likely be explained by the changing hydrogeological conditions resulting from the efforts of MCWD (e.g., Annexation Agreement, etc.) and others to reduce pumping in the coastal area. As a result, recharge from rainfall into the Dune Sand Aquifer creates a mound of freshwater that flows toward the Salinas River and the ocean.

We further note this protective condition is not isolated in a small area. This coastal condition was previously documented as part of the Fort Ord cleanup effort located southeast of the CEMEX site. The study named the aquitard layer the “Fort Ord-Salinas Valley Aquitard” (FO-SVA). Figure 5 - Perched Dune Sand Aquifer Schematic from Fort Ord Groundwater Monitoring Program shows a drawing of this condition, which was modified to illustrate groundwater flow directions (Ahtna, 2014).

**Figure 5 – Perched Dune Sand Aquifer Schematic
from Fort Ord Groundwater Monitoring Program**



This is a very significant development. Given that the groundwater found with a 36-foot elevation in the Dune Sand Aquifer at the location of MW-5S (and a 6-foot elevation at MW-7S), the Dune Sand Aquifer effectively provides a protective layer preventing seawater intrusion from moving into the Basin at a shallow depth and percolating downward into the underlying aquifers. Instead of allowing a shallow pathway for ocean water, the Dune Sand Aquifer having a potable fresh water quality based on its TDS concentration, appears to be slowly recharging the lower aquifers (i.e., the 180-Foot Aquifer and perhaps 400-Foot Aquifer), which has significantly reduced their TDS levels in this coastal area. This unique condition in the Marina Subarea is believed to provide recharge all along the coast in an area that effectively forms a linear recharge barrier within a mile of the shoreline. The extent of the Fort Ord-Salinas Valley Aquitard was estimated in a 2001 study conducted as part of the Fort Ord cleanup program (Harding ESE, 2001).

Monitoring data indicate that the elevation of the water levels in Monitoring Wells MW-7M and MW-8M are presently lower than the levels in both MW-4M and MW-5M. While the groundwater elevation is near mean sea level, the gradient indicated by the higher level at MW-5M shows that groundwater flows toward the coast up to MW-7 and MW-8 under these conditions. The significance is that after several years of drought conditions, the groundwater gradient between MW-4M (roughly ½ mile from the coast) and MW-5M (almost 2 miles from the coast) is relatively flat in the 180-FTE Aquifer. A significant decline in the groundwater level is observed to occur between MW-5M and MW-6M (see Figure 2). Further study would be required to understand if the mounding indicated in the 400-Foot Aquifer at MW-7 and MW-8 were from vertical recharge from the 180-FTE in this area along the coast.

III. Groundwater Quality Data

Water quality data developed as part of the test slant well project are summarized in the tables included in Attachment C – Laboratory Water Quality Test Results. The first table shown in Attachment C provides the only data published for wells other than the test slant well and MW-4 (Geoscience, 2015a). This table includes laboratory results for wells including MW-1, MW-3, MW-4, MW-5, and the test slant well. The second table in Attachment C is a compilation of laboratory data received by MCWD in October 2015 in response to a data request in the California Public Utilities Commission proceedings. This table includes data for monitoring wells MW-6, MW-7, MW-8, and MW-9 that to our knowledge, have not be published in any of the MPWSP documents.

The significance of these data is that they indicate beneficial conditions have developed (or have always existed) in the North Marina Area of the 180-400 Foot Aquifer Subbasin and may be contrary to information published by the Monterey County Water Resources Agency (MCWRA). The recent investigation that is being conducted in and around the North Marina Area as part of the MPWSP has discovered an occurrence of freshwater within the shallow Dune Sand Aquifer and the underlying 180-Foot Aquifer within the area delineated as seawater intruded by the MCWRA. As previously shown, water level data from wells in the shallow dune sand aquifer appear to show protective water levels that are sufficiently above sea level to prevent seawater intrusion in the shallower sediments. This condition, combined with the lack of pumping in the 180-Foot Aquifer in the North Marina Area, appears to have slowed seawater intrusion in this portion of the coastline. Water quality test results for total dissolved solids and chloride concentrations in these two uppermost aquifer zones are shown on Figures 6 and 7 – Average Total Dissolved Solids Concentrations in Groundwater and Average Chloride Concentrations in Groundwater, respectively.

These data suggest a change of groundwater conditions in this coastal section of the aquifer or alternatively, they may reveal the groundwater conditions that existed in an area largely lacking historical data. While the freshwater in this area contains salts and nutrients that are derived from overlying land uses that include agriculture, landfill, and wastewater treatment plant and composting facilities, the chemical character is not sodium chloride, which is indicative of seawater intrusion. Figure 8 and 9 – Stiff Diagrams of Dune Sand Aquifer Groundwater and 180-Foot Aquifer Groundwater, respectively show that the chemical character of groundwater in these new wells is predominantly calcium chloride and calcium bicarbonate. Additionally, elevated concentrations of nitrate are present in monitoring wells MW-5S, MW-7S and MW-8S and range from 115 mg/l to 237 mg/l. The concentration of nitrate decreases with depth at all of these sites, and is the highest at MW-5, which is closest to the landfill and the wastewater treatment facilities. Future use of this area for a direct potable groundwater supply may be unlikely; however, existing conditions do show abatement of seawater intrusion in the shallower aquifer zones in this coastal portion of the Salinas Valley Groundwater Basin. This condition may support the future beneficial uses of the 180-Foot Aquifer zone potentially including aquifer storage and recovery of highly purified recycled water for indirect potable reuse.

**Figure 6 – Average Total Dissolved Solids
 Concentrations in Groundwater**

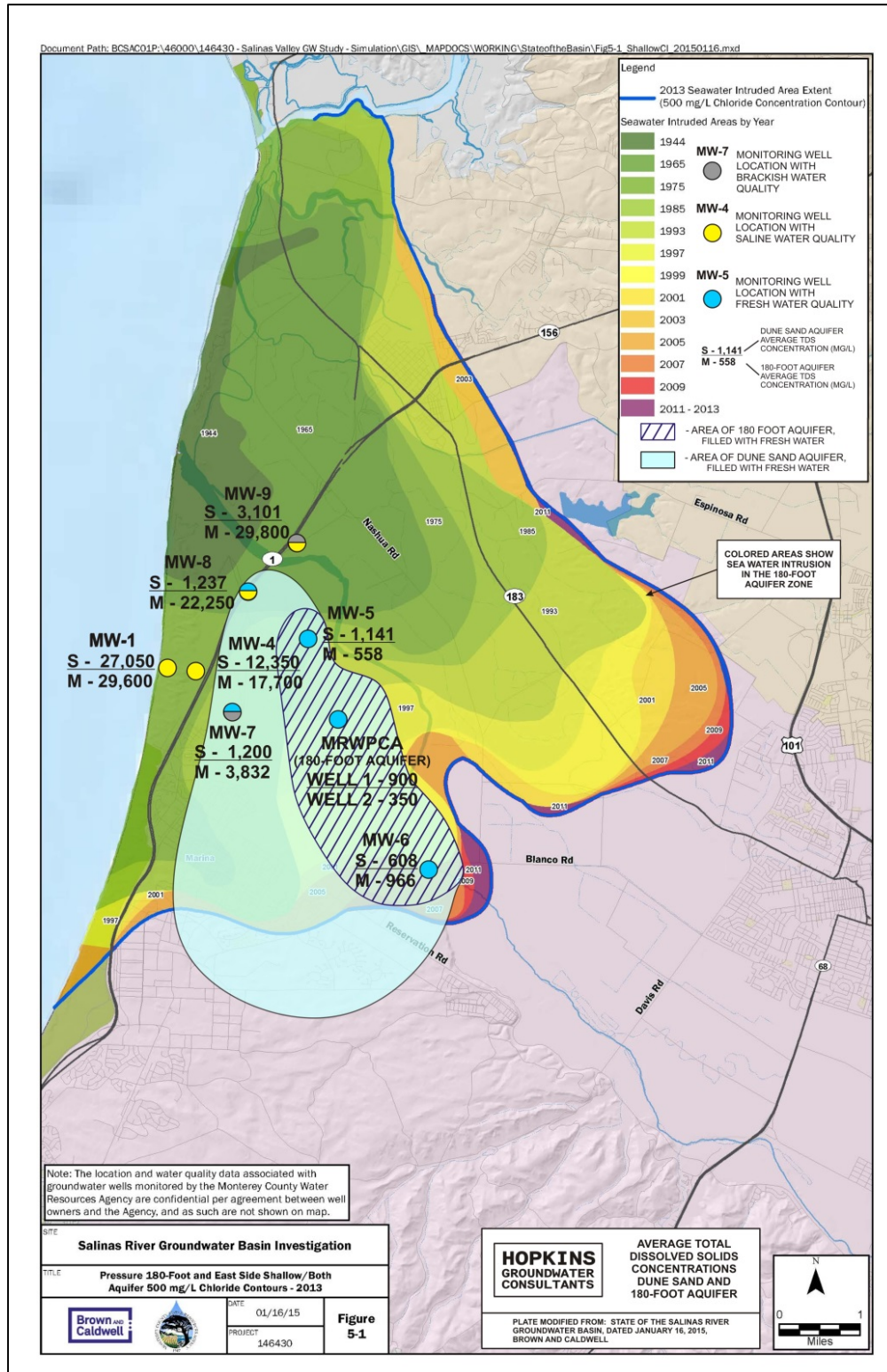


Figure 7 – Average Chloride Concentrations in Groundwater

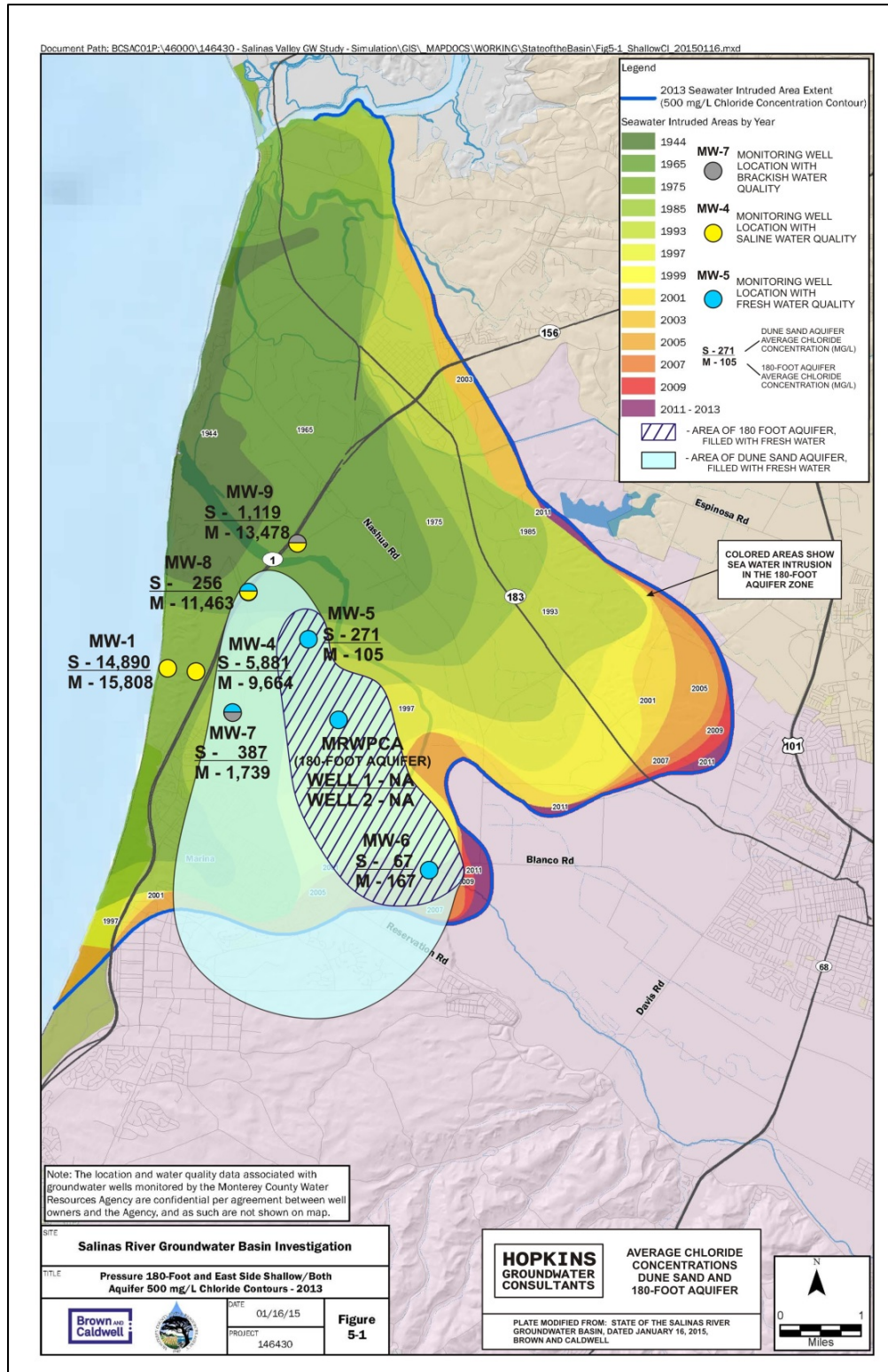


Figure 8 – Stiff Diagrams of Dune Sand Aquifer Groundwater

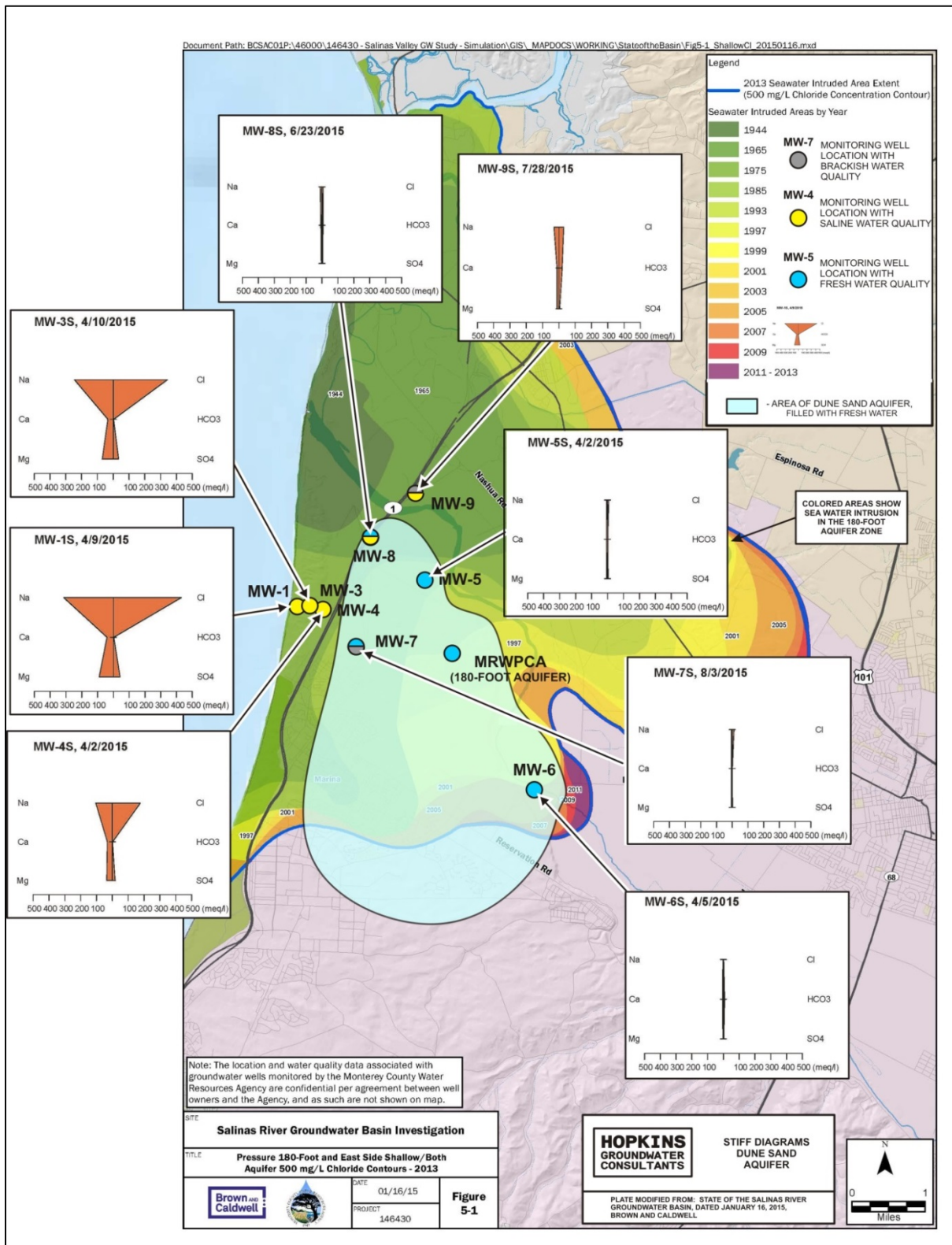
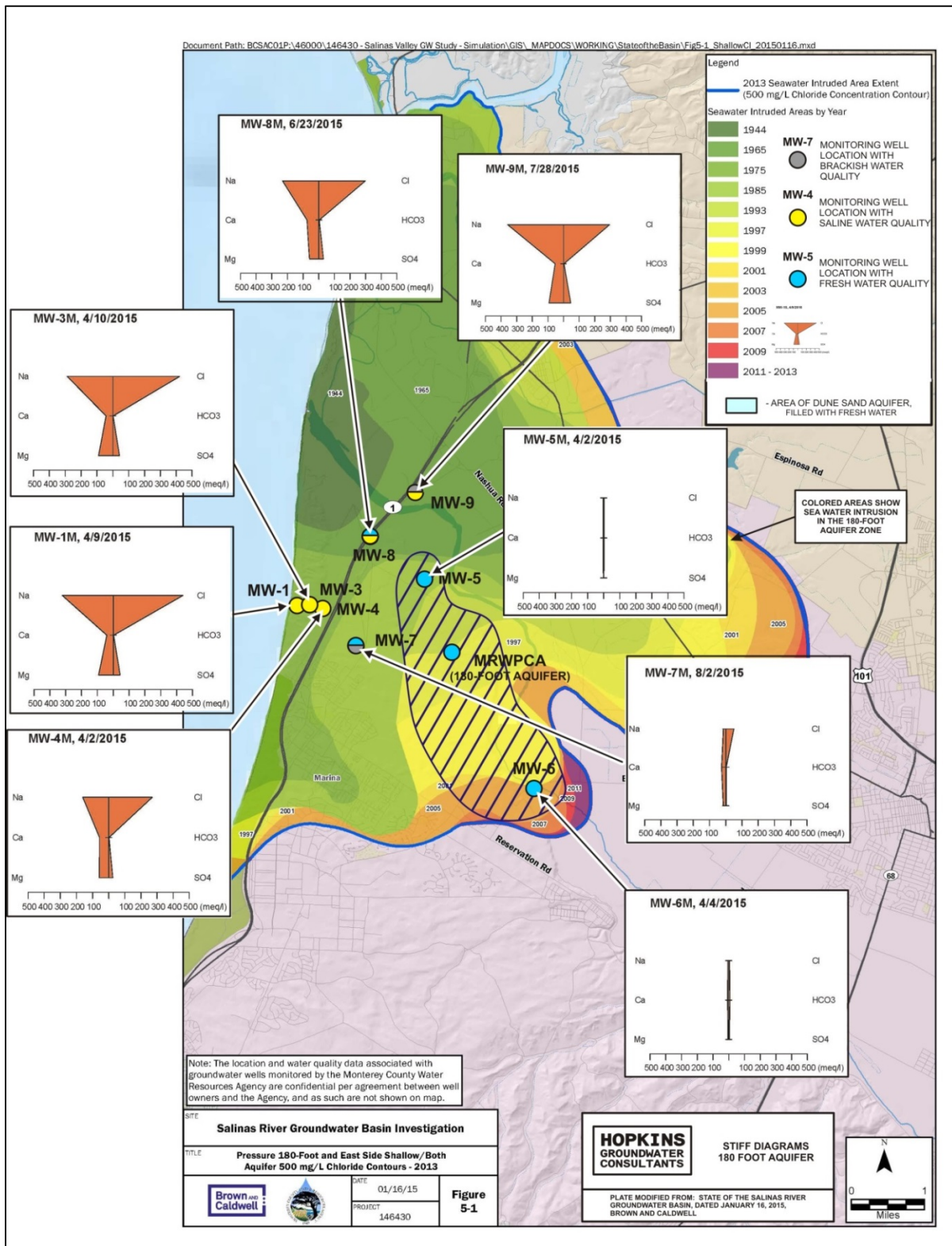


Figure 9 – Stiff Diagrams of 180-Foot Aquifer Groundwater

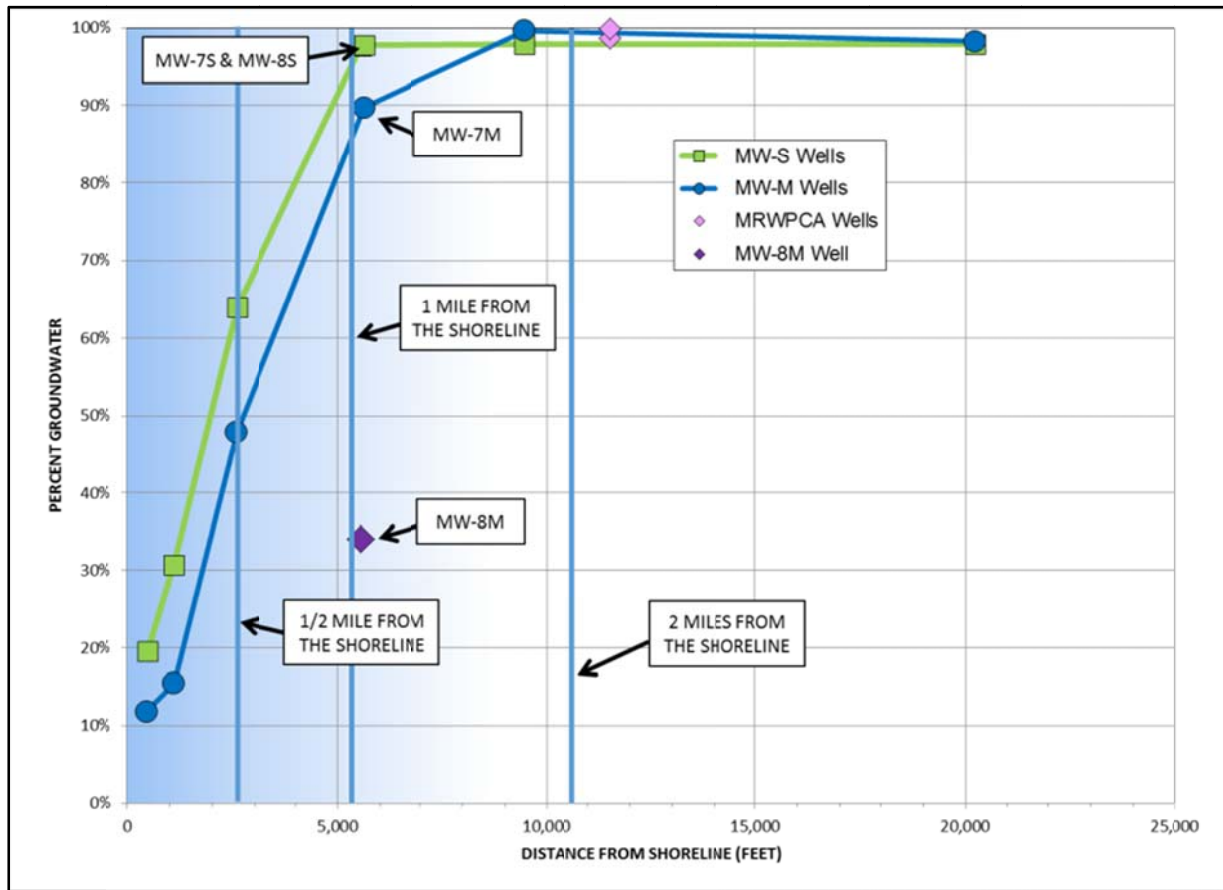


These data indicate a unique condition exists in the North Marina Subarea south of the Salinas River that provides a significant degree of protection against seawater intrusion in the shallower aquifers under the present and recent past hydrologic conditions. Figure 10 – Percent Groundwater with Distance From the Shoreline shows the rudimentary calculation of groundwater percentage versus ocean water percentage using the same equation applied to the test slant well discharge. The percentage of fresh groundwater in well water samples was calculated using the following equation:

$$GWP = [1 - (WSS - GWS / OWS - GWS)] \times 100$$

Where: GWP = Percent Groundwater
 WSS = Well Sample Salinity (mg/l)
 GWS = Groundwater Salinity (420 mg/l)
 OWS = Ocean Water Salinity (33,500 mg/l)

Figure 10 – Percent Groundwater with Distance From the Shoreline



Water quality data for this analysis were provided by the laboratory test results summarized in Attachment C. These available data show that the percentage of ocean water decreases significantly within a short distance from the coastline in the North Marina Area and the salinity of groundwater that is comparable to seawater is not up to 8 miles inland in the 180-Foot Aquifer as assumed by previous study. Calculation of percent ocean water using this method cannot differentiate between salts from overlying land uses and salt from ocean water. This calculation assumes that all salt in groundwater with a TDS above a concentration of 420 mg/l is from ocean water.

As shown in Figure 10, monitoring wells MW-5M and MW-6M along with the Monterey Regional Water Pollution Control Agency (MRWPCA) Wells are located in the 180-Foot Aquifer and the average TDS concentration for samples from these wells ranges from approximately 454 to 966 milligrams per liter (mg/l) and is also considered fresh water (See Figure 4 and Attachment C). However, the TDS concentration for MW-7M (3,832 mg/l) and MW-8M (22,250 mg/l) show that closer to the coast and closer to the main portion of the Basin north of the river, seawater has impacted the underlying 180-Foot Aquifer as shown in Figure 9 and 10.

We trust this review of available data provides a better understanding of what the MPWSP test slant well monitoring program has discovered. It is clear that without the new monitoring wells, this type of understanding about groundwater conditions in the North Marina Area could not have been provided from available data.

Sincerely,

HOPKINS GROUNDWATER CONSULTANTS, INC.



Curtis J. Hopkins

Principal Hydrogeologist

Certified Engineering Geologist, EG1800

Certified Hydrogeologist, HG114

Attachments: Plate 1 – Cross-Section A-A'

Plate 2 – Well Location Map

Attachment A – Well Construction Information

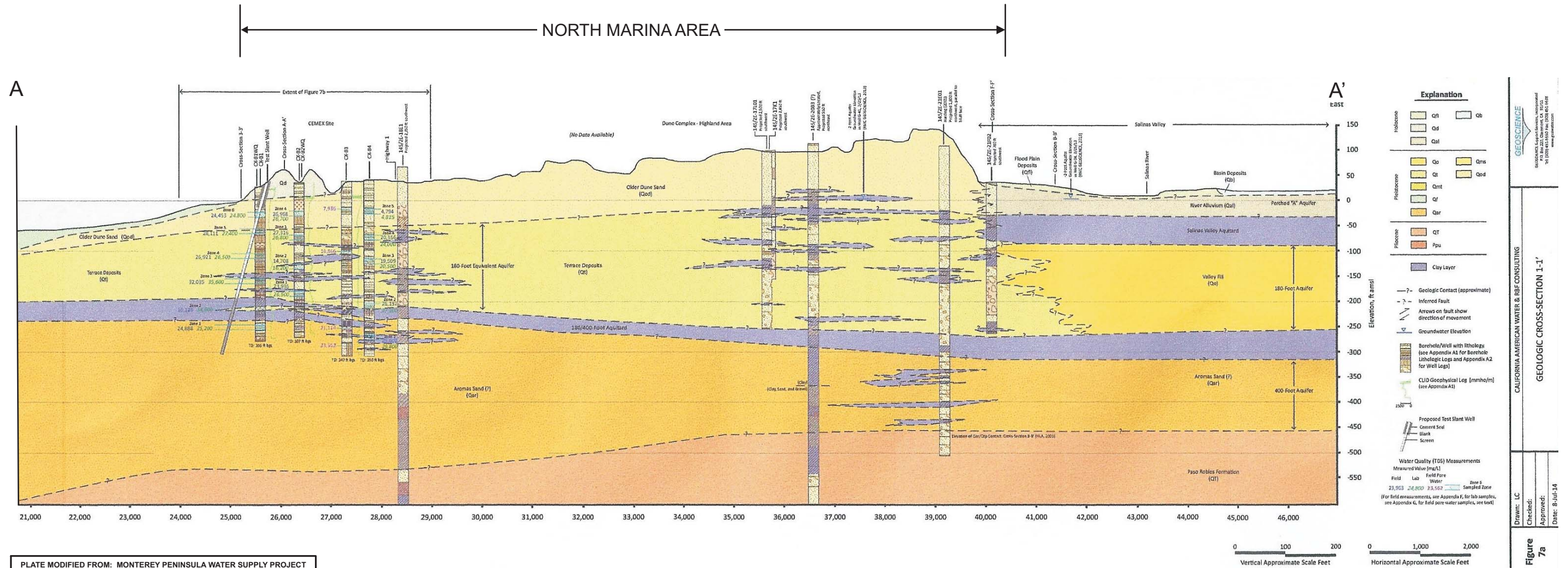
Attachment B – MPWSP Water Level Data

Attachment C – Laboratory Water Quality Test Results

References

- Ahtna Environmental Inc. (Ahtna, 2015), *Operable Unit Carbon Tetrachloride Plume Fourth Quarter 2014 Groundwater Monitoring Report, Former Fort Ord, California*, Prepared for Department of the Army, U.S. Army Corps of Engineers, Dated February.
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- Monterey County Water Resources Agency (MCWRA, 2014), *Historic Seawater Intrusion Map, Pressure 180-Foot Aquifer – 500 mg/L Chloride Areas and Pressure 400-Foot Aquifer*, Dated December 16.
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PLATES



GEOSCIENCE
 CALIFORNIA AMERICAN WATER & RFB CONSULTING
 GEOLOGIC CROSS-SECTION 1-1'
 Drawn: LC
 Checked:
 Approved:
 Date: 8-Jul-14

CROSS-SECTION A-A'
Technical Memorandum
 Marina Coast Water District
 Marina, California

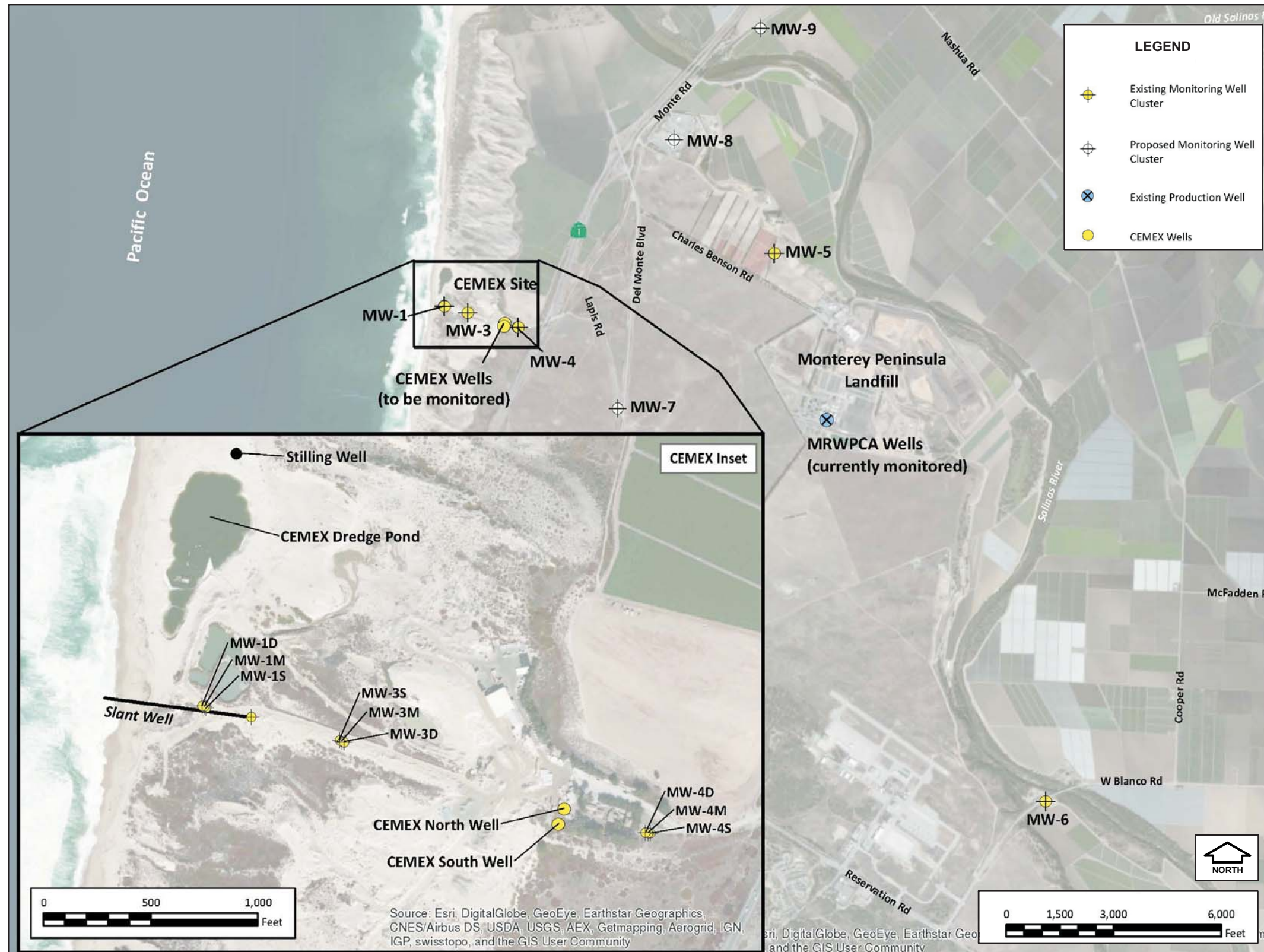


PLATE MODIFIED FROM: MONTEREY PENINSULA WATER SUPPLY PROJECT
TEST SLANT WELL LONG TERM PUMPING MONITORING REPORT NO. 55
DATED MAY 24, 2016, GEOSCIENCE SUPPLY SERVICES, INC.

WELL LOCATION MAP
Technical Memorandum
Marina Coast Water District
Marina, California

ATTACHMENT A
WELL CONSTRUCTION INFORMATION

Table 1: Well Information Table

| State Plane Coordinates | | | | | | | | | | | | | |
|-------------------------------|---------|-----------------------------|--------------|--------------|------------------------|-------------------------|--|--------------------------------------|---|--|-------------|-------------------------|---------------------|
| Well Name | Cluster | Reference Point (RP) | Northing | Easting | RP Elevation ft NAVD88 | RP Height (ft above GS) | Distance of RP from Slant Well Head (ft) | Top of Screen Interval (ft below GS) | Bottom of Screen Interval (ft below GS) | Transducer Installed Depth (ft below RP) | Survey Date | Data Logging Start Date | Data Collected |
| MW-1S | MW-1 | Top of ABS Transducer Mount | 2,154,745.35 | 5,739,355.82 | 30.51 ¹ | 2.65 ¹ | 211 | 55 | 95 | 76 | 26-Mar-15 | 19-Feb-15 | Level, Conductivity |
| MW-1M | MW-1 | Top of ABS Transducer Mount | 2,154,751.93 | 5,739,347.94 | 29.86 | 2.48 | 220 | 115 | 225 | 182 | 26-Mar-15 | 19-Feb-15 | Level, Conductivity |
| MW-1D | MW-1 | Top of ABS Transducer Mount | 2,154,753.60 | 5,739,337.98 | 29.68 ¹ | 2.65 ¹ | 230 | 277 | 327 | 309 | 26-Mar-15 | 19-Feb-15 | Level, Conductivity |
| MW-3S | MW-3 | Top of ABS Transducer Mount | 2,154,599.85 | 5,739,977.02 | 37.16 | 2.66 | 428 | 50 | 90 | 76 | 26-Mar-15 | 4-Mar-15 | Level, Conductivity |
| MW-3M | MW-3 | Top of ABS Transducer Mount | 2,154,592.96 | 5,739,988.54 | 37.35 | 2.73 | 441 | 105 | 215 | 182 | 26-Mar-15 | 4-Mar-15 | Level, Conductivity |
| MW-3D | MW-3 | Top of ABS Transducer Mount | 2,154,589.81 | 5,739,998.68 | 36.93 | 2.74 | 451 | 285 | 330 | 321 | 26-Mar-15 | 4-Mar-15 | Level, Conductivity |
| MW-4S | MW-4 | Top of ABS Transducer Mount | 2,154,170.90 | 5,741,427.62 | 41.96 | 2.26 | 1,940 | 60 | 100 | 66 | 26-Mar-15 | 9-Mar-15 | Level, Conductivity |
| MW-4M | MW-4 | Top of ABS Transducer Mount | 2,154,172.79 | 5,741,416.78 | 41.99 | 2.15 | 1,929 | 130 | 260 | 208 | 26-Mar-15 | 9-Mar-15 | Level, Conductivity |
| MW-4D | MW-4 | Top of ABS Transducer Mount | 2,154,174.30 | 5,741,406.08 | 41.95 | 2.15 | 1,918 | 290 | 330 | 317 | 26-Mar-15 | 20-Feb-15 | Level, Conductivity |
| MW-5S | MW-5 | Top of ABS Transducer Mount | 2,156,239.19 | 5,748,566.86 | 80.25 ¹ | 2.20 ¹ | 9,135 | 43 | 83 | 71 | 26-Mar-15 | 10-Mar-15 | Level, Conductivity |
| MW-5M | MW-5 | Top of ABS Transducer Mount | 2,156,230.38 | 5,748,564.26 | 80.48 ¹ | 2.31 ¹ | 9,131 | 100 | 310 | 171 | 26-Mar-15 | 10-Mar-15 | Level, Conductivity |
| MW-5D | MW-5 | Top of ABS Transducer Mount | 2,156,220.77 | 5,748,560.95 | 80.06 | 1.97 | 9,126 | 395 | 435 | 417 | 26-Mar-15 | 19-Feb-15 | Level, Conductivity |
| MW-6S | MW-6 | Top of ABS Transducer Mount | 2,141,142.87 | 5,756,164.01 | 35.89 | 2.45 ¹ | 21,436 | 30 | 60 | 61 | 1-Oct-15 | 22-Apr-15 | Level, Conductivity |
| MW-6M | MW-6 | Top of ABS Transducer Mount | 2,141,138.40 | 5,756,154.35 | 35.68 | 2.44 ¹ | 21,431 | 150 | 210 | 103 | 1-Oct-15 | 22-Apr-15 | Level, Conductivity |
| MW-6D | MW-6 | Top of ABS Transducer Mount | 2,141,133.06 | 5,756,144.94 | 35.82 | 2.42 ¹ | 21,427 | 255 | 325 | 201 | 1-Oct-15 | 22-Apr-15 | Level, Conductivity |
| MW-7S | MW-7 | Top of ABS Transducer Mount | 2,152,099.25 | 5,744,148.10 | 50.64 | 2.06 | 5,274 | 60 | 80 | 72 | 1-Oct-15 | 13-Aug-15 | Level, Conductivity |
| MW-7M | MW-7 | Top of ABS Transducer Mount | 2,152,110.46 | 5,744,146.08 | 50.29 | 2.09 | 5,266 | 130 | 220 | 187 | 1-Oct-15 | 13-Aug-15 | Level, Conductivity |
| MW-7D | MW-7 | Top of ABS Transducer Mount | 2,152,120.50 | 5,744,144.38 | 50.24 | 2.24 | 5,260 | 295 | 345 | 322 | 1-Oct-15 | 13-Aug-15 | Level, Conductivity |
| MW-8S | MW-8 | Top of ABS Transducer Mount | 2,159,440.33 | 5,744,871.52 | 19.96 | 2.14 ³ | 7,116 | 40 | 80 | - | 1-Oct-15 | 30-May-15 | Hand Level |
| MW-8M | MW-8 | Top of ABS Transducer Mount | 2,159,430.86 | 5,744,866.05 | 19.99 | 2.17 ² | 7,106 | 125 | 215 | 181 | 1-Oct-15 | 30-May-15 | Level, Conductivity |
| MW-8D | MW-8 | Top of ABS Transducer Mount | 2,159,421.47 | 5,744,861.04 | 20.08 | 2.10 ³ | 7,096 | 300 | 350 | - | 1-Oct-15 | 30-May-15 | Hand Level |
| MW-9S | MW-9 | Top of ABS Transducer Mount | 2,162,010.77 | 5,747,345.03 | 18.42 | 2.16 ³ | 10,677 | 30 | 110 | - | 1-Oct-15 | 1-Jul-15 | Hand Level |
| MW-9M | MW-9 | Top of ABS Transducer Mount | 2,162,016.58 | 5,747,353.64 | 18.32 | 2.13 ² | 10,687 | 145 | 225 | 182 | 1-Oct-15 | 29-Jun-15 | Level, Conductivity |
| MW-9D | MW-9 | Top of ABS Transducer Mount | 2,162,022.89 | 5,747,362.25 | 18.32 | 2.15 ³ | 10,697 | 353 | 393 | - | 1-Oct-15 | 26-Jun-15 | Hand Level |
| Well No. 1 ⁴ | MRWPCA | Well Cover | 2,151,622.14 | 5,750,015.59 | 114 ft amsl (GS) | 1.60 | 10,898 | 260 | 340 | 299 | - | 19-Feb-15 | Level, Conductivity |
| Well No. 2 ⁴ | MRWPCA | Well Cover | 2,151,550.18 | 5,749,987.41 | 115 ft amsl (GS) | 1.65 | 10,892 | 260 | 340 | 319 | - | 19-Feb-15 | Level, Conductivity |
| CEMEX Dredge Pond | CEMEX | Top of ABS Transducer Mount | 2,155,912.41 | 5,739,497.26 | 14.14 | 8.92 [*] | 1,212 | - | - | - | 26-Mar-15 | 8-Mar-15 | Level, Conductivity |
| Test Slant Well | CEMEX | Near Ground Surface | 2,154,702.56 | 5,739,561.92 | 30.86 | 0 | 0 | 46 ^{**} | 231 ^{**} | 305MD | 26-Mar-15 | 1-Apr-15 | Level, Conductivity |
| CEMEX North Well | CEMEX | Well Cover | 2,154,284.48 | 5,741,032.07 | 39.20 | 0.25 | 1,529 | 244 | 481 | 150 | 1-Oct-15 | 1-Apr-15 | Level, Conductivity |
| CEMEX South Well ⁴ | CEMEX | Ground Surface | 2,154,213.90 | 5,740,998.57 | 31 ft amsl (GS) | 0 | 1,518 | 400 | 506 | - | - | - | - |

Horizontal Datum: NAD83 State Plane Zone 4
 Vertical Datum: NAVD88
¹ RP/elevation change on May 17, 2015 - New caps
² RP/elevation change on July 17, 2015 - New caps
³ RP/elevation change on September 24, 2015 - New caps
⁴ Estimated - not surveyed.
 MD: Measured Depth - lineal feet along the angle of the slant well
 GS: Ground Surface - approximate ground surface elevation based on Google Earth
^{*} RP height above pond water level 5.22 ft NAVD88 (8-11 am 26-Mar-15)
^{**} Top of 18 in. screen = 140 ft x Sin(19) = 46 ft TVD, Bottom of 14 in. screen = 710 x Sin(19) = 231 ft TVD

ATTACHMENT B
MPWSP WATER LEVEL DATA

Groundwater Elevation in MPWSP MW-1

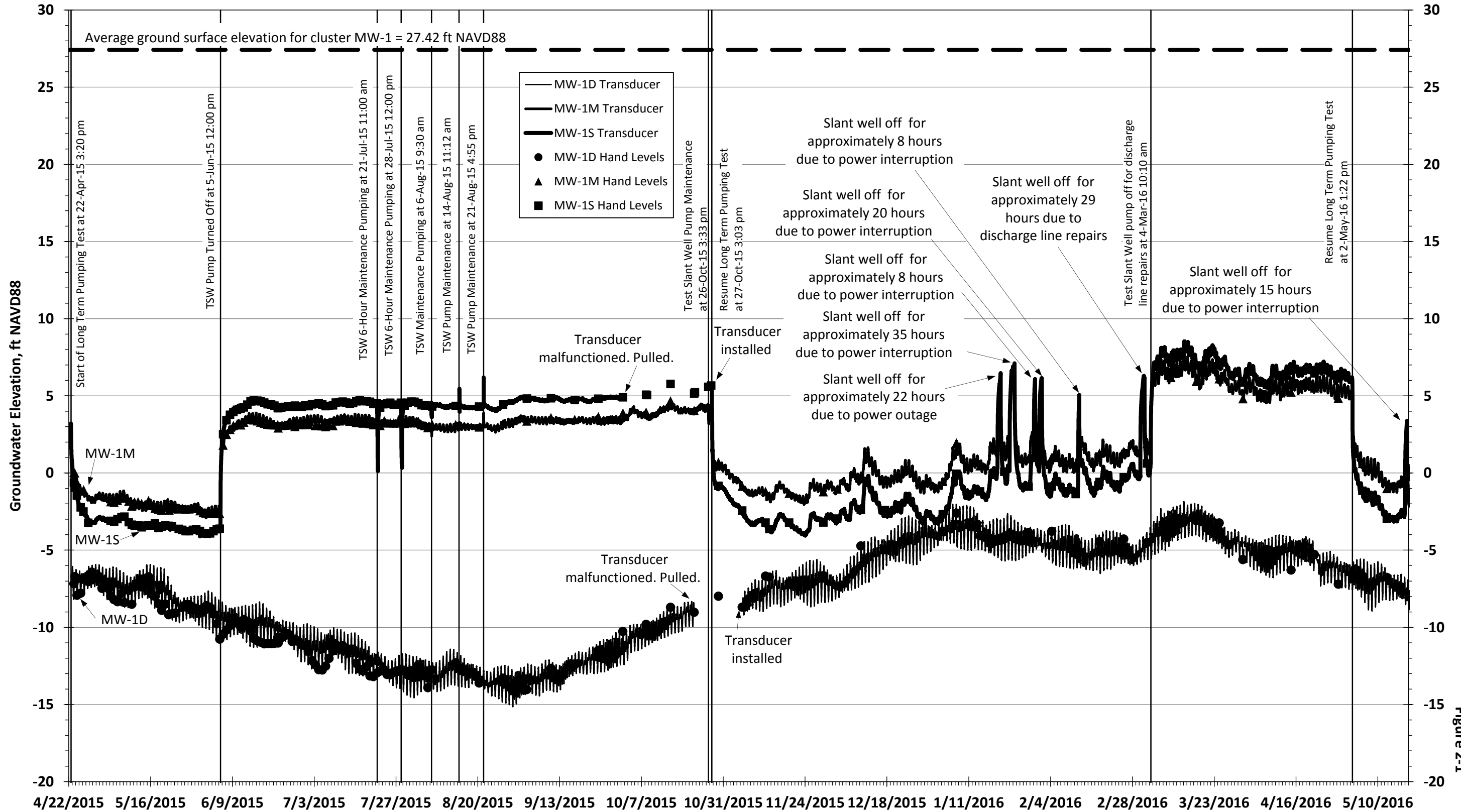


Figure 2-1

Groundwater Elevation in MPWSP MW-3

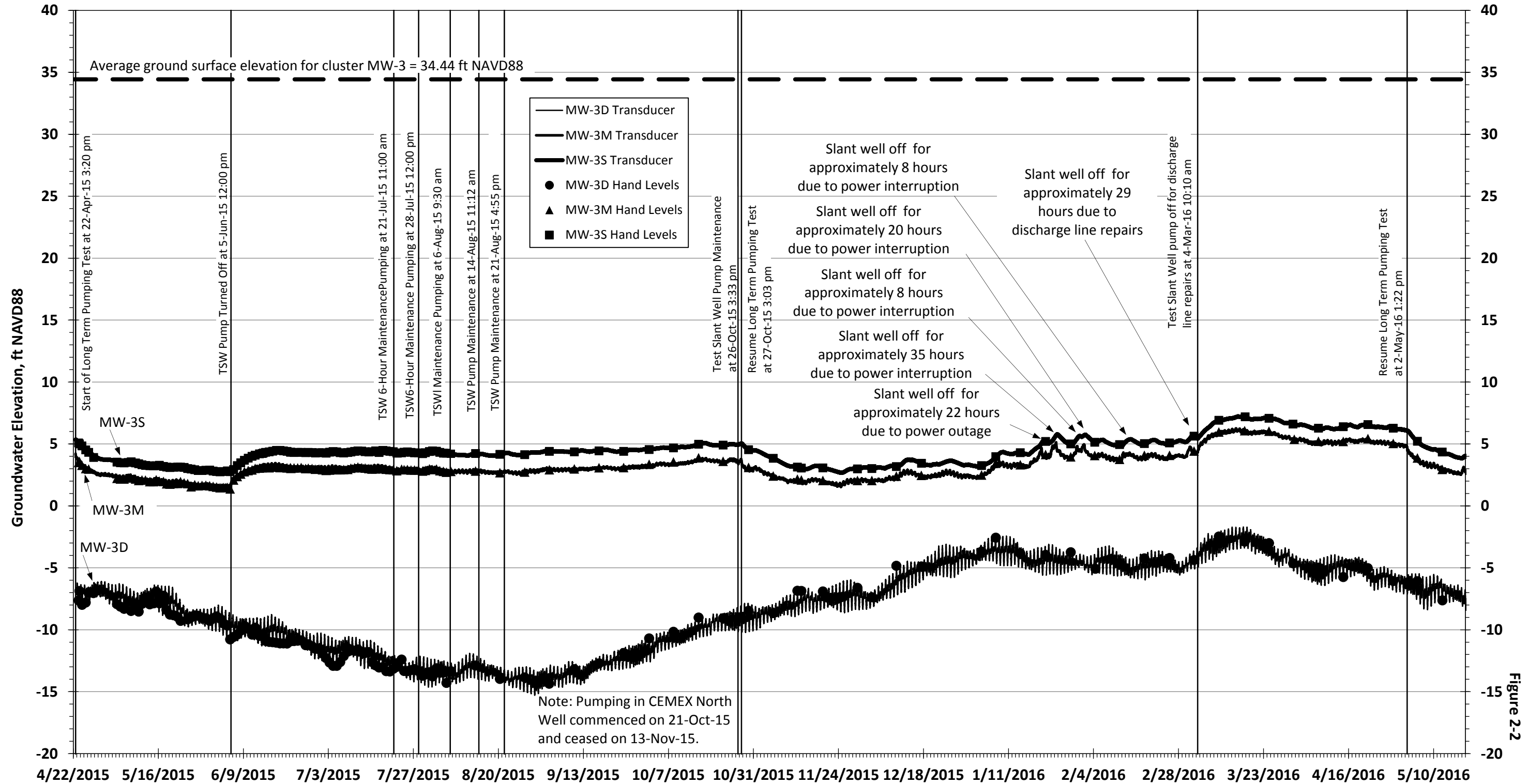


Figure 2-2

Groundwater Elevation in MPWSP MW-4

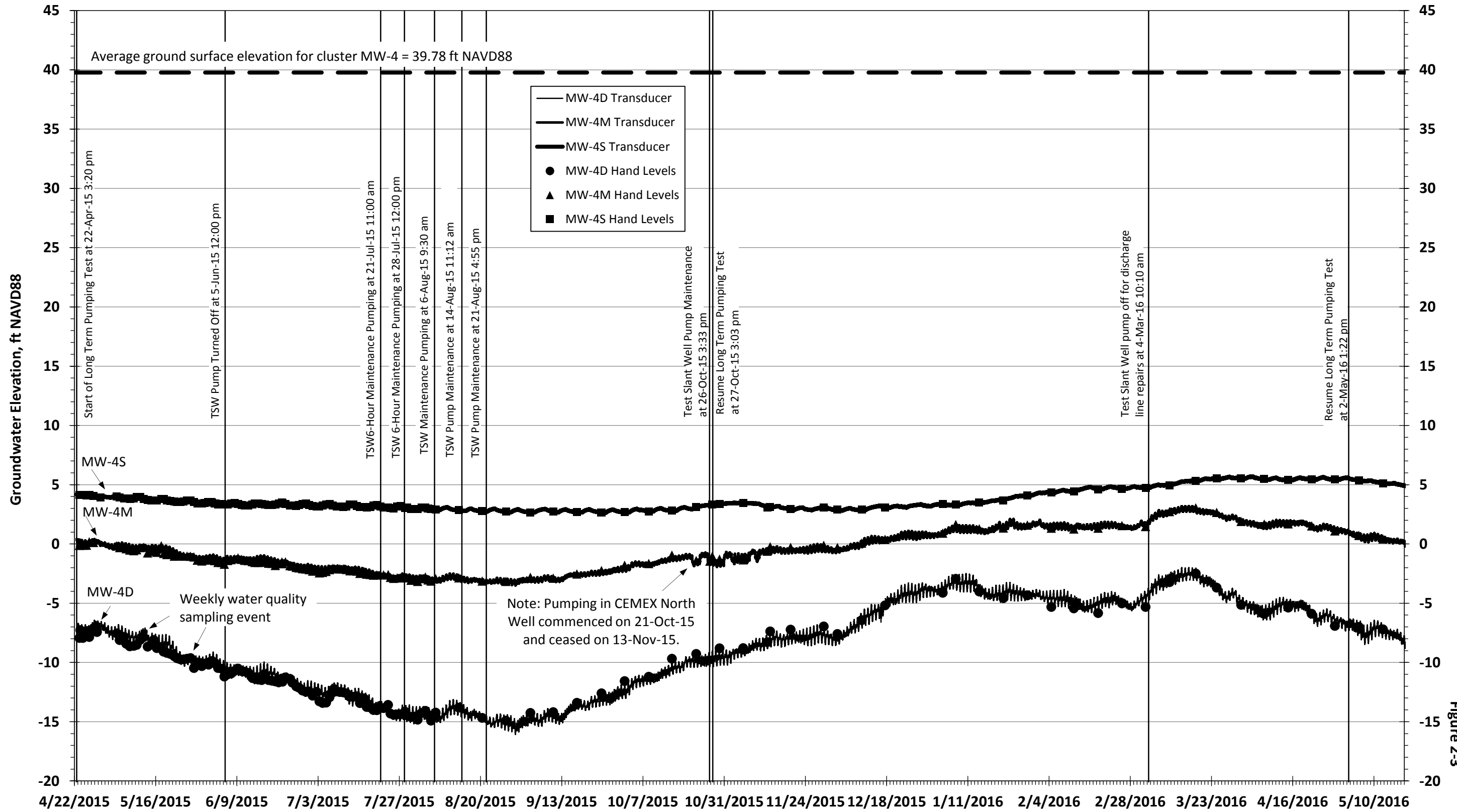


Figure 2-3

Groundwater Elevation in MPWSP MW-5

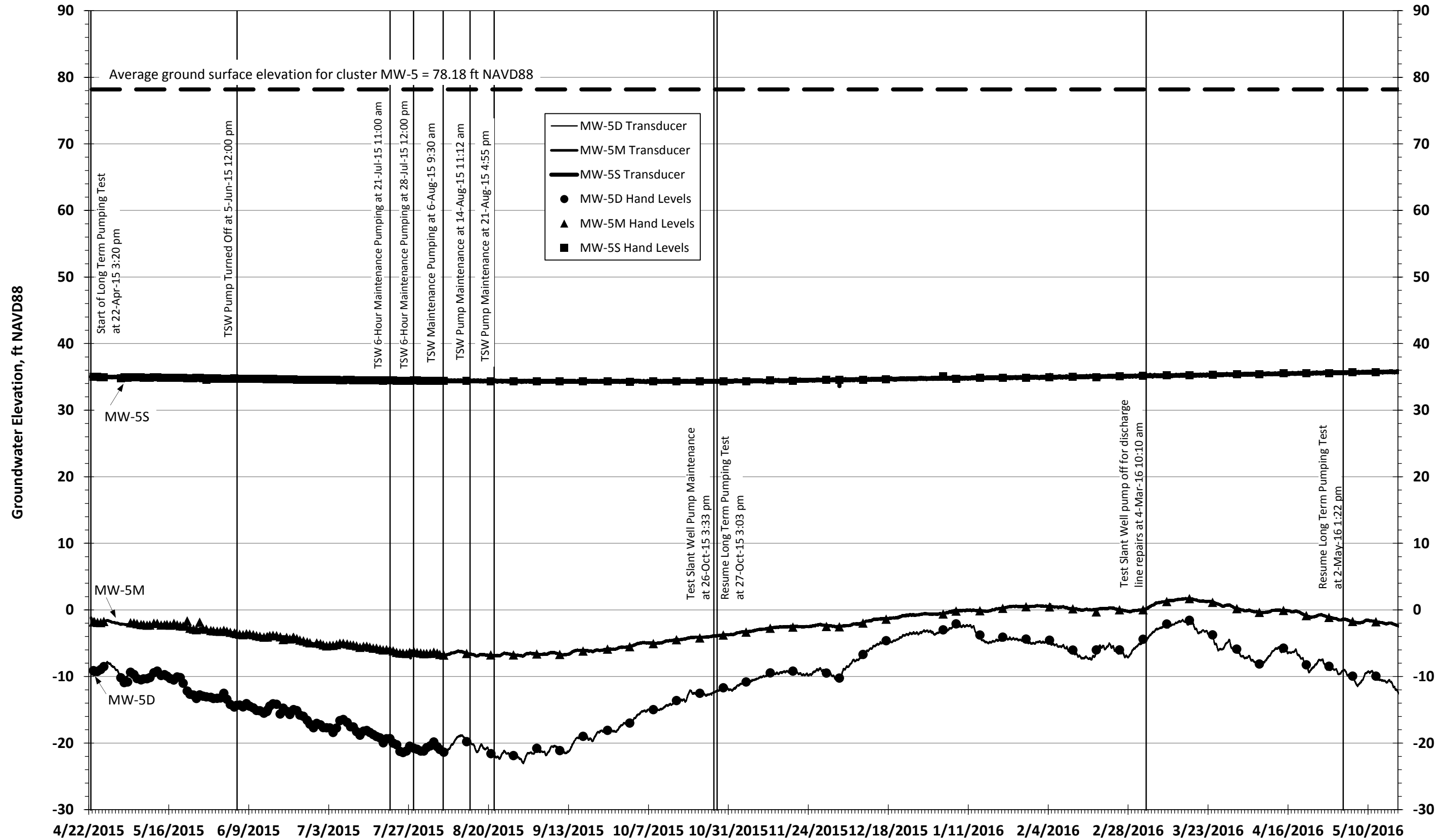


Figure 2-4

Groundwater Elevation in MPWSP MW-6

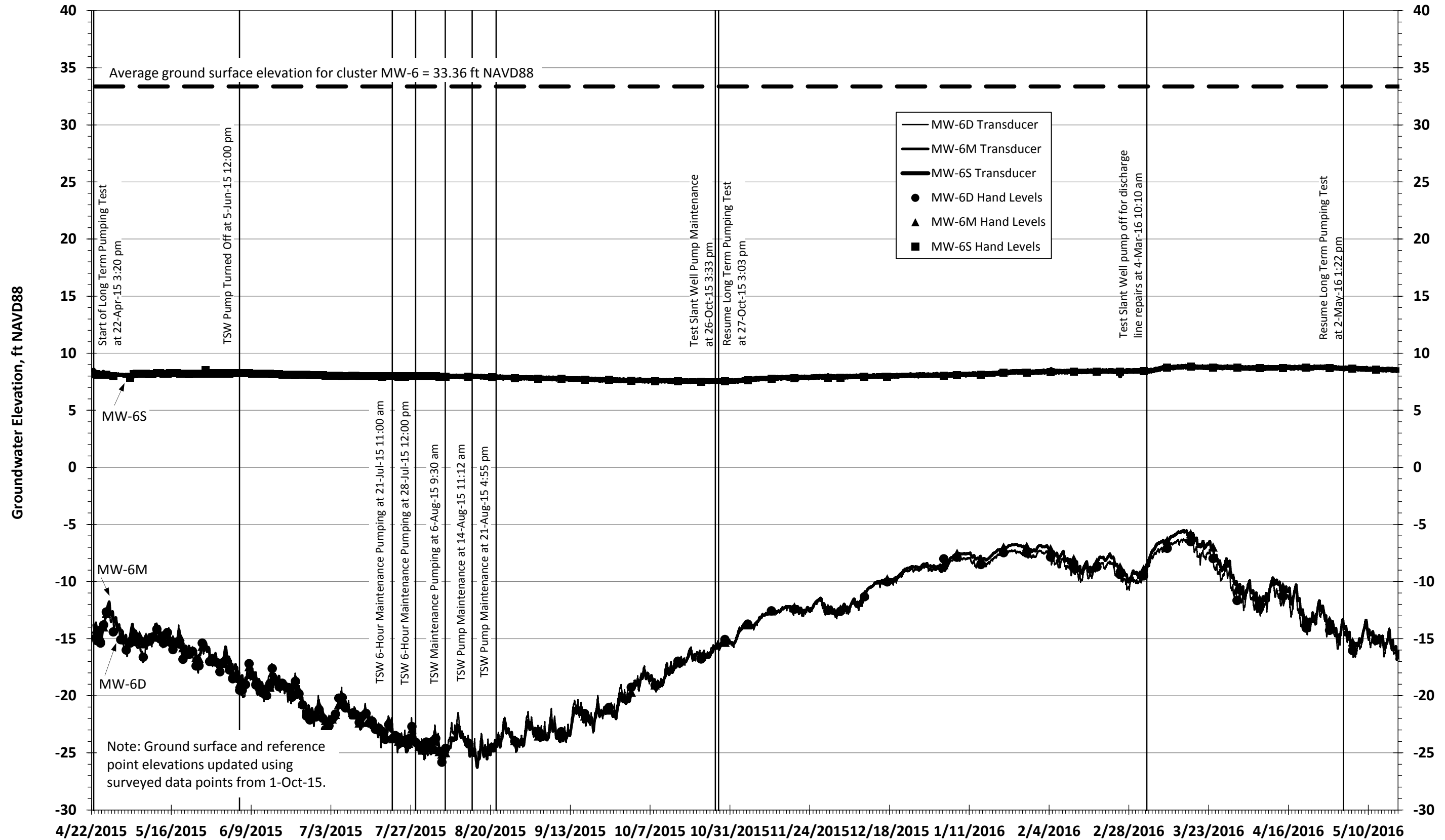


Figure 2-5

Groundwater Elevation in MPWSP MW-7

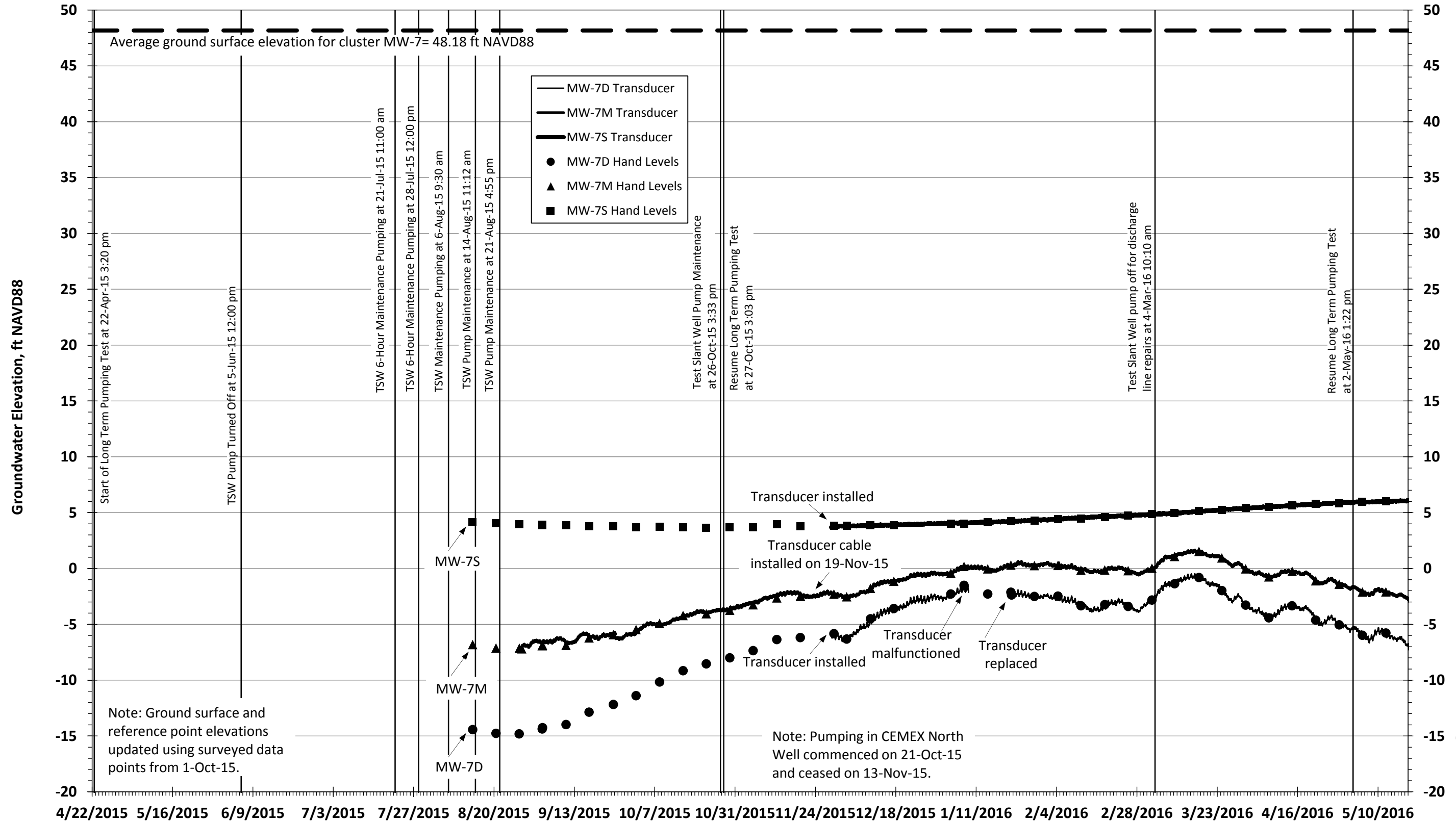


Figure 2-6

Groundwater Elevation in MPWSP MW-8

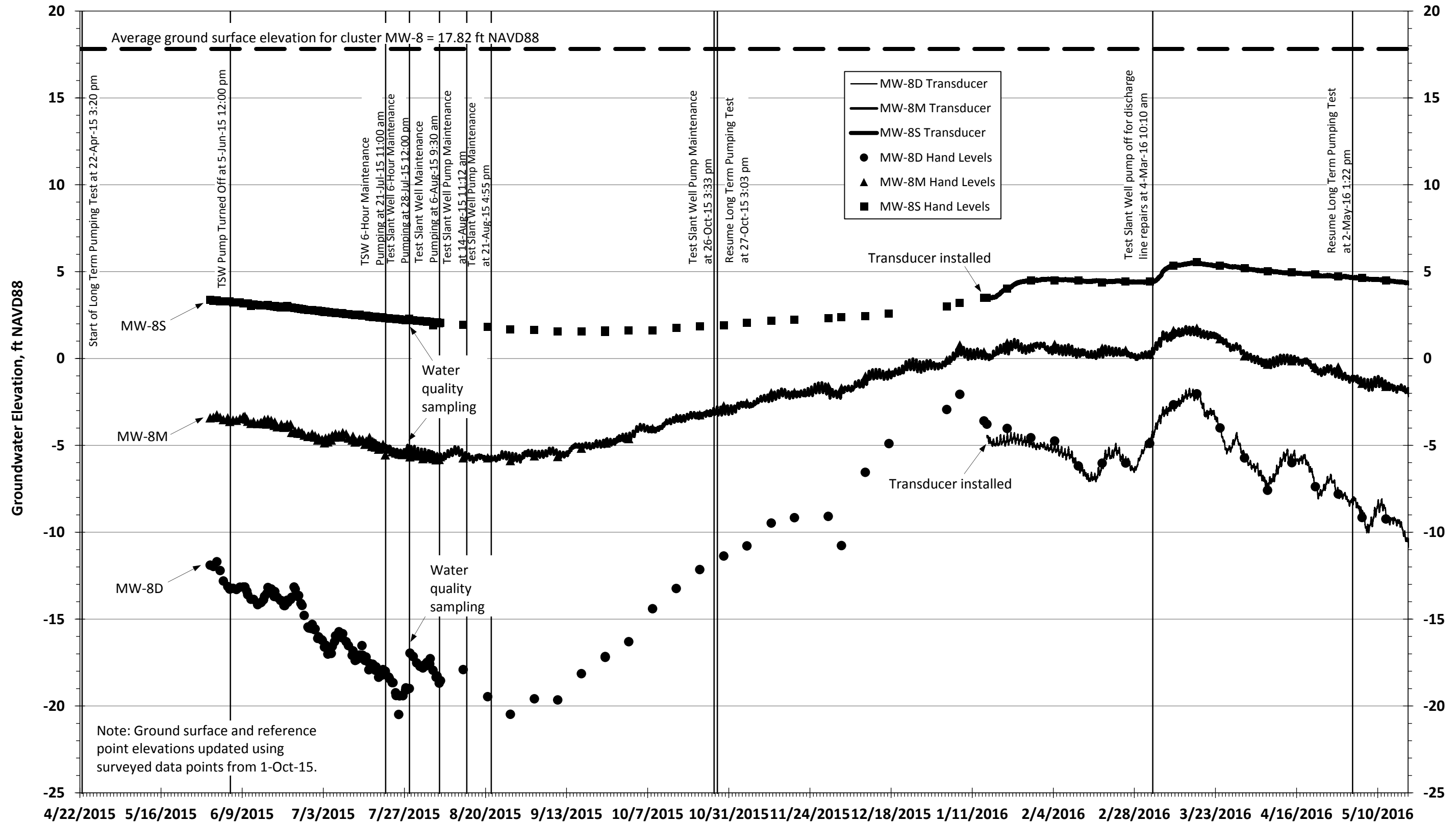


Figure 2-7

Groundwater Elevation in MPWSP MW-9

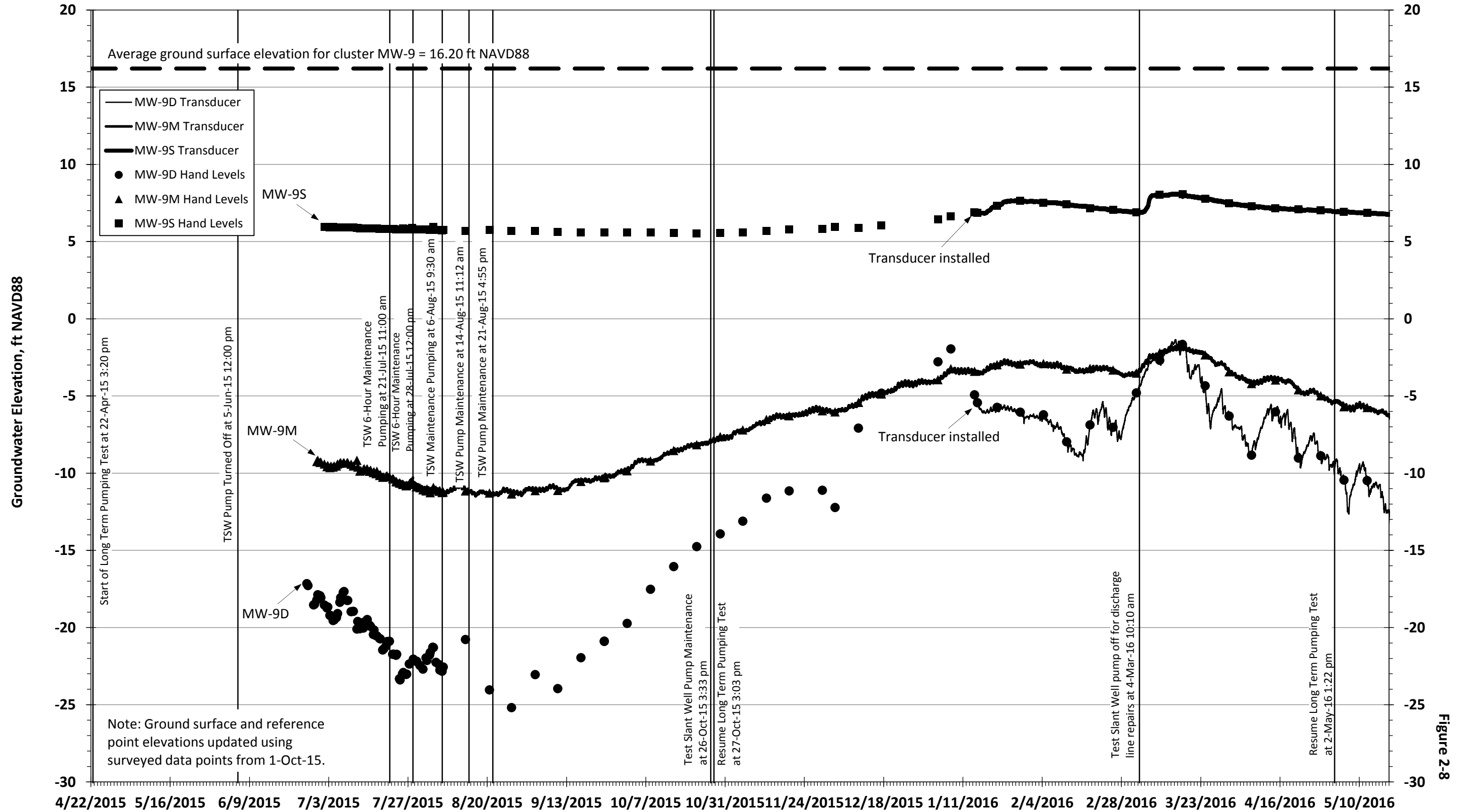


Figure 2-8

Groundwater Elevation in Monterey Regional Water Pollution Control Agency Wells

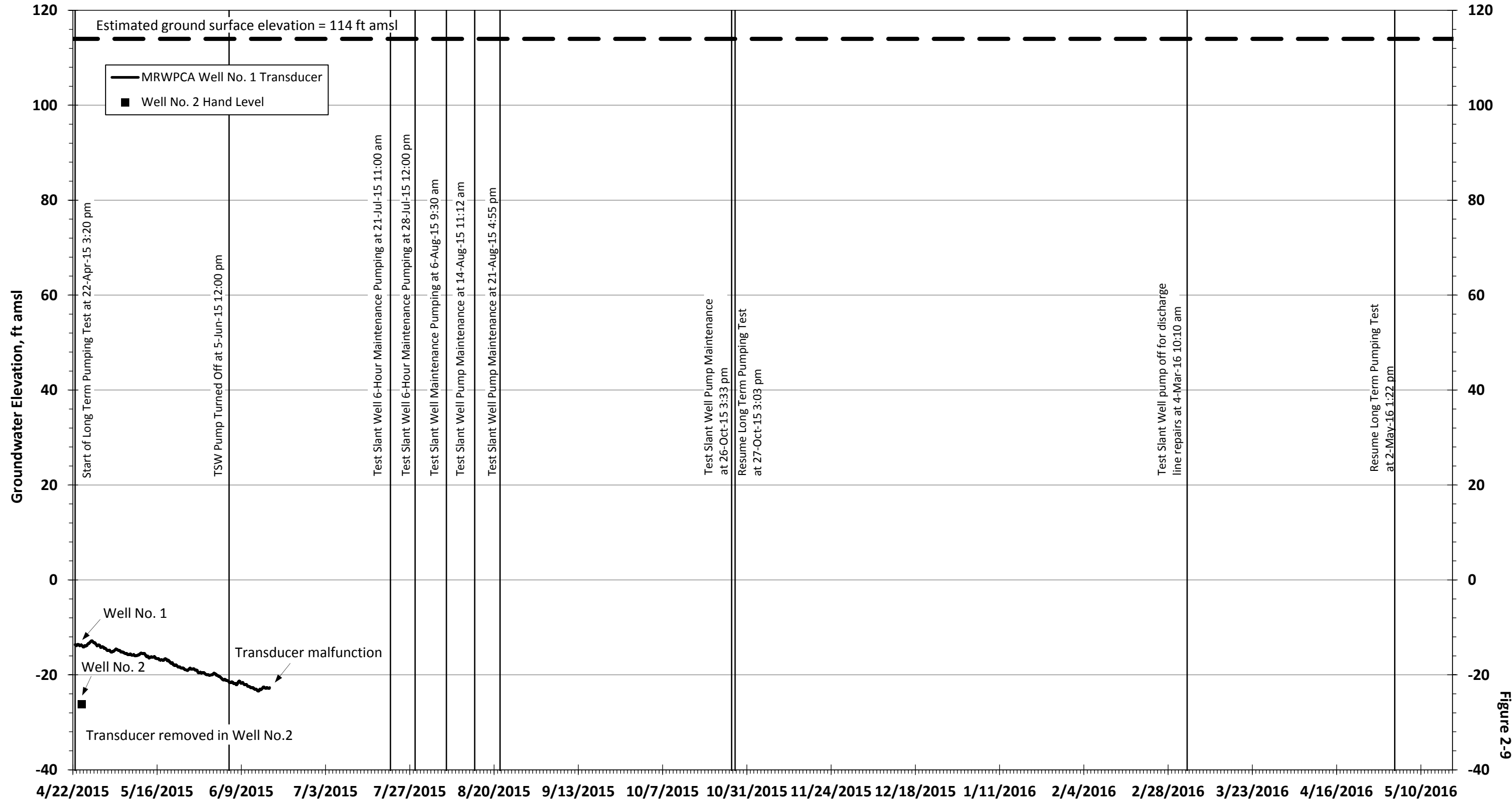


Figure 2-9

Surface Water Elevation in CEMEX Dredge Pond

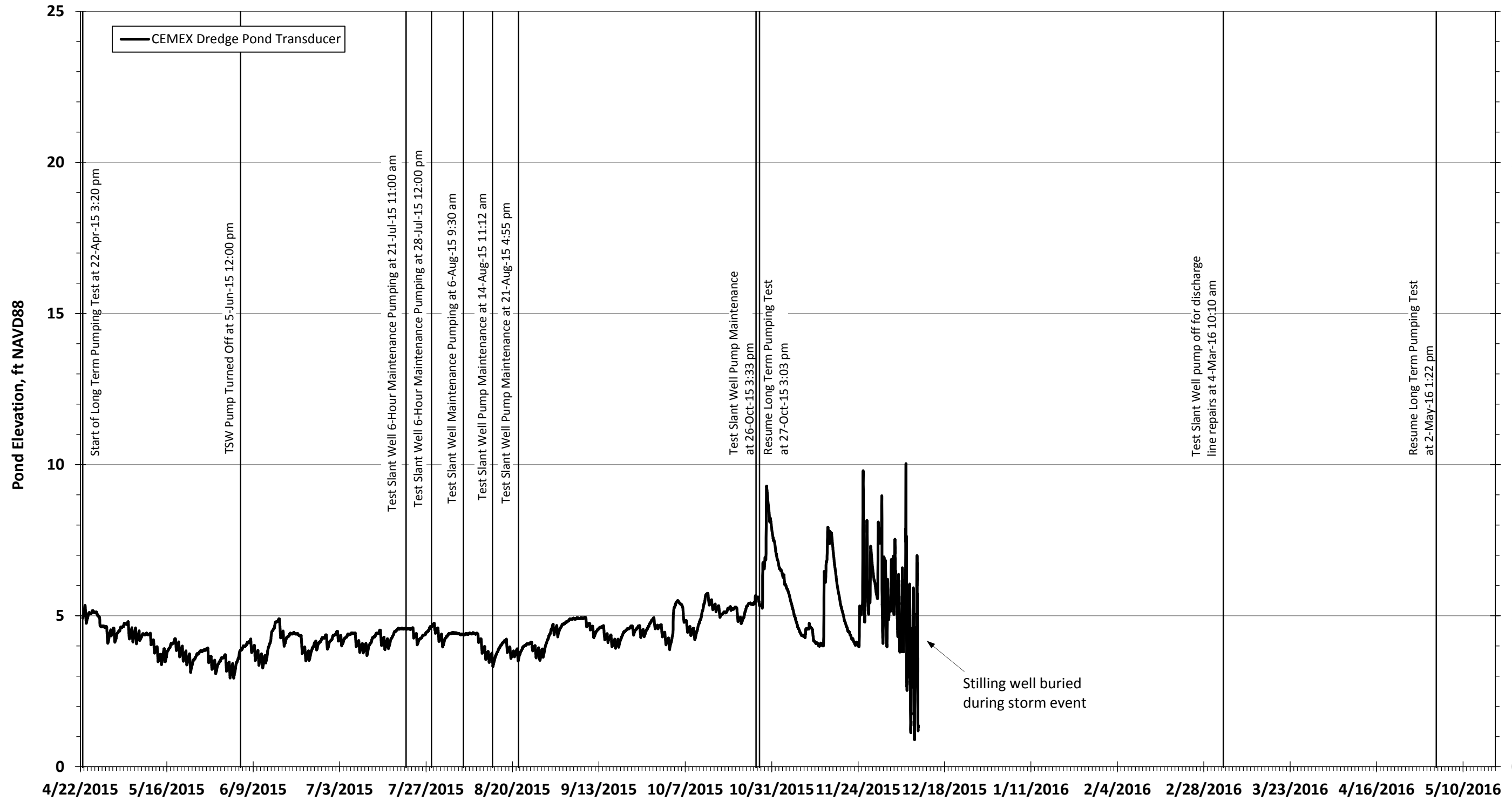


Figure 2-10

Groundwater Elevation in CEMEX North Well

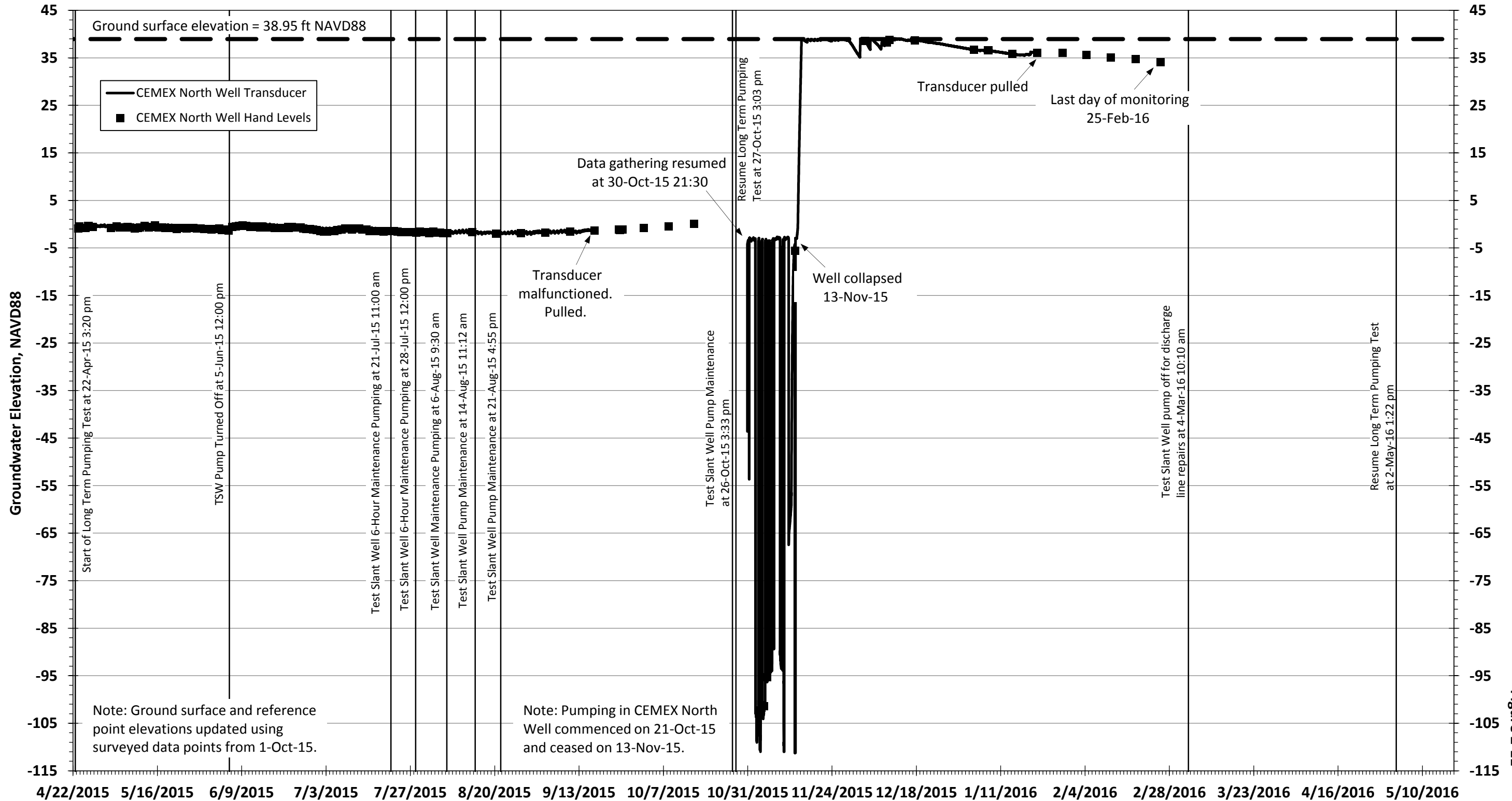


Figure 2-11

Groundwater Elevation in MPWSP Test Slant Well

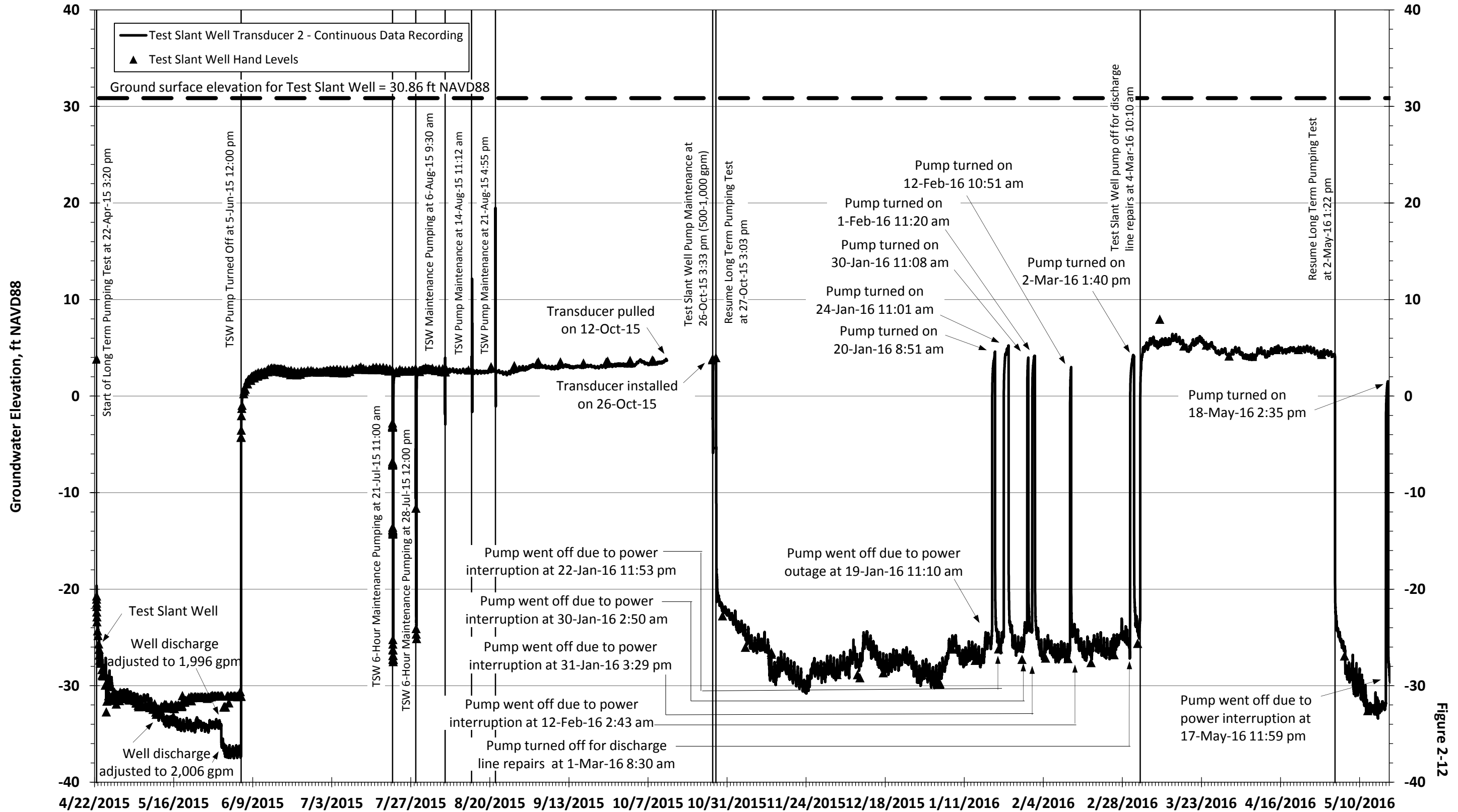


Figure 2-12

**ATTACHMENT C
LABORATORY WATER QUALITY
TEST RESULTS**

Cal Am / RBF
 Baseline Water and Total Dissolved Solids Levels
 Monterey Peninsula Water Supply Project Area

Table 2

Summary of Laboratory Water Quality Results in Monitoring Wells

| Well Name: | MW-1D | MW-1M | MW-1S | MW-3D | MW-3M | MW-3S | MW-4D | MW-4M | MW-4S | MW-5D | MW-5M | MW-5S | Test Slant Well | | | | | | | | | | | | | | | |
|-------------------------------|-----------|-----------|-----------|-----------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|---------------------------|----------|----------|----------|----------|----------|-----------|----------|----------|----------|-----------|----------|-----------|-----------|----------|--------|
| Screen Interval (ft bgs): | 277 - 327 | 115 - 225 | 55 - 95 | 285 - 330 | 105 - 215 | 50 - 90 | 280 - 330 | 100 - 230 | 50 - 90 | 380 - 430 | 100 - 325 | 50 - 90 | 140 - 320, 400 - 710 (MD) | | | | | | | | | | | | | | | |
| Sample Date: | 14-Feb-15 | 9-Apr-15 | 14-Feb-15 | 9-Apr-15 | 13-Feb-15 | 9-Apr-15 | 21-Feb-15 | 10-Apr-15 | 24-Feb-15 | 10-Apr-15 | 25-Feb-15 | 10-Apr-15 | 19-Feb-15 | 2-Apr-15 | 6-Mar-15 | 2-Apr-15 | 7-Mar-15 | 2-Apr-15 | 17-Feb-15 | 2-Apr-15 | 3-Mar-15 | 2-Apr-15 | 10-Mar-15 | 2-Apr-15 | 20-Mar-15 | 24-Mar-15 | 8-Apr-15 | |
| Constituent ¹ | Units | Result | Result | Result | Result | Result | Result | Result | Result | Result | Result | Result | Result | Result | Result | Result | Result | Result | Result | Result | Result | Result | Result | Result | Result | Result | Result | |
| Sulfate | mg/L | 1,950 | N/A | 2,070 | N/A | 1,840 | N/A | N/A | N/A | N/A | N/A | N/A | 1,700 | N/A | N/A | N/A | N/A | N/A | 58 | 1,700 | N/A | N/A | N/A | N/A | N/A | N/A | N/A | |
| Sulfate, Dissolved | mg/L | N/A | 2,148 | N/A | 2,048 | N/A | 2,008 | 2,058 | 2,158 | 1,960 | 1,967 | 1,533 | 1,605 | N/A | 1,796 | 1,184 | 1,205 | 716 | 807 | N/A | 31 | 110 | 67 | 197 | 192 | N/A | 1,840 | |
| Temperature | ° C | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | 16.3 | N/A | |
| Temperature (Field) | ° C | 19.2 | 20.02 | 17.2 | 17.89 | 18.8 | 17.64 | 19.6 | 20.22 | 16.3 | 18.74 | 17.5 | 19.17 | 19.9 | 19.8 | 18.4 | 18.3 | 17.7 | 18.1 | 21.3 | 21.4 | 16.97 | 18.2 | 16.7 | 18.1 | 20.9 | 19.1 | 17.2 |
| Total Diss. Solids | mg/L | 29,100 | 28,700 | 30,900 | 28,300 | 26,600 | 27,500 | 32,600 | 28,600 | 28,500 | 28,300 | 23,400 | 23,300 | 27,500 | 27,600 | 17,900 | 17,500 | 11,900 | 12,800 | 2,616 | 2,437 | 663 | 454 | 1,166 | 1,117 | 25,300 | 24,400 | 25,400 |
| Total Susp. Solids | mg/L | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | 36 | ND | N/A |
| Turbidity | NTU | 1.8 | 0.15 | 0.1 | 0.1 | 0.1 | 0.15 | 1 | 0.3 | 0.1 | 0.16 | 0.15 | 0.24 | 0.65 | 0.15 | 0.25 | 0.05 | 0.3 | 0.2 | 0.25 | 0.25 | ND | ND | 0.4 | 0.75 | 17 | 1.6 | 0.4 |
| Turbidity (Field) | NTU | 0.65 | 0.69 | 0.41 | 0.35 | 0.28 | 0.43 | 0.38 | 0.87 | 0.42 | 0.21 | 0.96 | 0.55 | 0.76 | 0.53 | 0.71 | 0.84 | 0.52 | 0.17 | 0.71 | 0.87 | 0.47 | 0.45 | 1.31 | 1.26 | 40.3 | 0.66 | 0.74 |
| Volatile Org. Compounds (524) | µg/L | ND | N/A | ND | N/A | ND | N/A | ND | N/A | ND | N/A | RP | N/A | RP | N/A | ND | N/A | RP | N/A | RP | N/A | ND | N/A | RP | N/A | N/A | N/A | ND |
| Zinc, Total | µg/L | ND | ND | ND | ND | 413 | ND | ND | ND | 297 | ND | 312 | ND | ND | ND | 211 | 107 | ND | 108 | 51 | ND | 40 | ND | 43 | ND | N/A | N/A | ND |

Notes:

- °C = Degrees Celsius
- CU = Color Units
- mg/L = Milligrams per Liter
- NTU = Nephelometric Turbidity Units
- µg/L = Picograms per Liter
- TON = Threshold Odor Number
- µg/L = Micograms per Liter
- µmhos/cm = Micromhos per Centimeter
- H = Analyzed outside of hold time
- MPN/100mL = The most probable number (MPN) of coliform or fecal coliform bacteria per 100 milliliter
- ND = NOT DETECTED at or above the Reporting Limit or Practical Quantitation Limit. If J-value reported, then NOT DETECTED at or above the Method Detection Limit (MDL)
- N/A = No Lab Results available
- RP = Results to be provided

¹ Laboratory water quality reports will be provided in the Test Slant Well and monitoring well completion report.
^{*} Laboratory water quality results pending.

| CONSTITUENT | UNIT | MW-6D | MW-6M | MW-6S | MW-7D | MW-7M | MW-7S | MW-8D | MW-8D | MW-8M | MW-8M | MW-8S | MW-8S | MW-9D | MW-9D | MW-9M | MW-9M | MW-9S | MW-9S |
|---|-----------|----------|----------|----------|----------|----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| | | 4/2/2015 | 4/4/2015 | 4/5/2015 | 9-Aug-15 | 2-Aug-15 | 3-Aug-15 | 5/21/2015 | 6/23/2015 | 5/27/2015 | 6/23/2015 | 5/28/2015 | 6/23/2015 | 25-Jun-15 | 28-Jul-15 | 28-Jun-15 | 28-Jul-15 | 30-Jun-15 | 28-Jul-15 |
| ALKALINITY, TOTAL (as CaCO ₃) | mg/L | 117 | 397 | 366 | 109 | 98 | 29 | 152 | 112 | 140 | 155 | 320 | 302 | 170 | 176 | 127 | 128 | 1,051 | 1,019 |
| ALUMINUM, TOTAL | µg/L | ND | ND | ND | ND | 18 | ND | 37 | 128 | 292 | ND | ND | ND | ND | ND | ND | ND | 11 | ND |
| AMMONIA-N | mg/L | NA | NA | NA | | | | NA | NA | NA | NA | NA | NA | | | | | | |
| AMMONIA-N, DISSOLVED | mg/L | ND | 0.17 | 0.45 | ND | ND | 0.08 | ND | ND | ND | ND | ND | ND | ND | 0.07 | 0.12 | 0.17 | 2.83 | 2.86 |
| AMMONIA-NH ₃ (CALC) UN-IONIZED | ug/L | NA | NA | NA | | | | NA | NA | NA | NA | NA | NA | | | | | | |
| ARSENIC, TOTAL | µg/L | 3 | 5 | 16 | 41 | 4 | 1 | 1 | 11 | 28 | 24 | 1 | 1 | 2 | 2 | 39 | 35 | 11 | 12 |
| BARIUM, DISSOLVED | µg/L | 255 | 155 | 105 | 110 | 282 | 199 | 88 | 178 | 154 | 119 | 57 | 75 | 59 | 48 | 163 | 141 | 315 | 273 |
| BICARBONATE (AS HCO ₃ ⁻) | mg/L | 143 | 484 | 447 | 133 | 120 | 35 | 185 | 137 | 171 | 189 | 390 | 368 | 207 | 215 | 155 | 156 | 1,282 | 1,243 |
| BORON, DISSOLVED | mg/L | ND | ND | ND | 1.71 | ND | ND | 0.05 | 0.66 | 1.83 | 1.37 | 0.22 | 0.29 | 0.08 | 0.07 | 2.93 | 2.77 | 0.69 | 0.64 |
| BROMIDE, DISSOLVED | mg/L | 2 | 0.5 | 0.2 | 44.3 | 6.6 | 1.3 | 0.6 | 11.5 | 42.1 | 33.6 | 0.9 | 1 | 0.2 | 0.2 | 49.6 | 47.6 | 4.2 | 3.5 |
| CALCIUM | mg/L | 341 | 139 | 93 | 1,900 | 507 | 120 | 64 | 413 | 1110 | 1500 | 149 | 142 | 32 | 34 | 878 | 1,060 | 209 | 234 |
| CALCIUM, DISSOLVED | mg/L | 347 | 140 | 92 | 1,890 | 520 | 114 | 59 | 416 | 1140 | 1500 | 151 | 139 | 35 | 33 | 869 | 1,100 | 242 | 235 |
| CARBAMATES BY HPLC (EPA 531) | µg/L | ND | ND | ND | ND | ND | ND | ND | ND | NA | ND | ND | ND | ND | | ND | ND | ND | ND |
| CARBONATE AS CaCO ₃ | mg/L | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND |
| CHLORIDE, DISSOLVED | mg/L | 814 | 167 | 57 | 13,589 | 1,739 | 387 | 220 | 3995 | 12380 | 10546 | 261 | 251 | 74 | 75 | 16,519 | 10,436 | 1,199 | 1,038 |
| CHLORINATED PESTICIDES AND PCB (EPA 508) | µg/L | ND | A | A | A | ND | ND | ND | ND | ND | ND | A | A | ND | | ND | | ND | |
| CHLORINE RESIDUAL, TOTAL (LABORATORY) | mg/L (H) | NA | NA | NA | | | | | NA | NA | NA | NA | NA | | | | | | |
| COLIFORM, E. COLI (QUANTITRAY) | MPN/100ml | NA | NA | NA | | | | | NA | NA | NA | NA | NA | | | | | | |
| COLIFORM, E. COLI (QUANTITRAY) - 18 HOUR | MPN/100ml | NA | NA | NA | | | | | NA | NA | NA | NA | NA | | | | | | |
| COLIFORM, TOTAL (QUANTITRAY) | MPN/100ml | NA | NA | NA | | | | | NA | NA | NA | NA | NA | | | | | | |
| COLIFORM, TOTAL (QUANTITRAY) - 18 HOUR | MPN/100ml | NA | NA | NA | | | | | NA | NA | NA | NA | NA | | | | | | |
| COLOR, APPARENT (UNFILTERED) | CU | 5 | 16 | 20 | ND | ND | ND | 11 | 16 | ND | 7 | 3 | ND | ND | 3 | 6 | 14 | 175 | 60 |
| COPPER, TOTAL | µg/L | 8 | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | 10 | ND | ND | ND | ND | ND |
| DBCP & EDB | µg/L | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND |
| DIOXIN | pg/L | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND |
| DIQUAT (EPA 549) | µg/L | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND |
| DISSOLVED OXYGEN (FIELD) | mg/L (H) | NA | NA | NA | | | | | NA | NA | NA | NA | NA | | | | | | |
| DISSOLVED OXYGEN (LABORATORY) | mg/L (H) | NA | NA | NA | | | | | NA | NA | NA | NA | NA | | | | | | |
| ENDOTHALL | µg/L | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | | ND | | ND | |
| FLUORIDE, DISSOLVED | mg/L | 0.1 | ND | 0.2 | ND | ND | 0.1 | 0.3 | ND | 0.4 | ND | 0.1 | ND | 0.3 | 0.3 | ND | ND | ND | 0.4 |
| GLYPHOSATE | µg/L | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | | ND | | ND | |
| HARDNESS (AS CaCO ₃) | mg/L | 1222 | 565 | 393 | 9,030 | 2,044 | 547 | 263 | 2057 | 6080 | 6698 | 578 | 556 | 133 | 138 | 6,718 | 7,296 | 1,218 | 1,206 |
| HYDROXIDE | mg/L | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND |
| IODIDE | µg/L | ND | 35 | 35 | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | 500 | 330 |
| IRON | µg/L | ND | 184 | 315 | ND | ND | 33 | 81 | 274 | ND | ND | 104 | ND | 10 | ND | 670 | 1,540 | 6,964 | 6,878 |
| IRON, DISSOLVED | µg/L | ND | 182 | 315 | ND | ND | 26 | 15 | ND | ND | ND | 99 | ND | ND | ND | 667 | 1,520 | 6,300 | 1,400 |
| KIEHLDAHL NITROGEN, DISSOLVED | mg/L | ND | 0.7 | 1 | ND | ND | 0.09 | ND | ND | ND | ND | ND | ND | ND | 0.11 | 0.2 | 0.19 | 6.12 | 2.9 |
| LITHIUM | µg/L | 25 | 17 | 6 | 271 | 29 | 5 | 49 | 157 | 132 | 132 | ND | 6 | 38 | 39 | 289 | 296 | 23 | 20 |
| MAGNESIUM | mg/L | 90 | 53 | 39 | 1,040 | 189 | 60 | 25 | 249 | 801 | 717 | 50 | 49 | 13 | 13 | 1,100 | 1,130 | 169 | 151 |
| MAGNESIUM, DISSOLVED | mg/L | 83 | 49 | 37 | 1,010 | 192 | 58 | 23 | 250 | 828 | 692 | 51 | 47 | 13 | 13 | 1,090 | 1,140 | 161 | 152 |
| MANGANESE, DISSOLVED | µg/L | 714 | 821 | 2090 | 230 | 372 | 476 | 283 | 759 | 353 | 642 | ND | 76 | 247 | 186 | 1,120 | 1,410 | 4,920 | 4,830 |
| MANGANESE, TOTAL | µg/L | 750 | 810 | 1880 | 232 | 372 | 500 | 310 | 847 | 354 | 668 | ND | 86 | 254 | 188 | 1,160 | 1,380 | 5,140 | 4,840 |
| MBAS (SURFACTANTS) | mg/L | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND |
| NITRATE AS NO ₃ | mg/L | 2 | ND | ND | 6 | 15 | 198 | 2 | 6 | 5 | 6 | 123 | 115 | 2 | 2 | 5 | 6 | ND | ND |
| NITRATE+NITRITE AS N | mg/L | 0.7 | 0.5 | 0.5 | 1.4 | 3.4 | 44.8 | 0.7 | 1.3 | 1.5 | 1.4 | 28.2 | 26.8 | 0.9 | 0.8 | 1.2 | 1.3 | 2.5 | 1.2 |
| NITRITE AS NO ₂ -N, DISSOLVED | mg/L | 0.2 | 0.1 | 0.5 | ND | ND | 0.1 | 0.3 | ND | 0.4 | ND | 0.4 | 0.8 | 0.3 | 0.3 | ND | ND | 2.5 | 1.2 |
| ODOR THRESHOLD AT 60 C | TON | 1 | 1 | 2 | 1 | 2 | 2 | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 | 1 | 2 | 2 | 5 |
| OIL & GREASE (HEM) | mg/L | NA | NA | NA | | | | | NA | NA | NA | NA | NA | | | | | | |
| o-PHOSPHATE-P | mg/L | 0.05 | 0.32 | 1.55 | 0.05 | 0.016 | 0.035 | 0.06 | 0.04 | 0.06 | 0.04 | 0.1 | 0.13 | 0.06 | 0.13 | 0.06 | 0.04 | 1.34 | 0.28 |
| pH (FIELD TEST) | pH | 7.24 | 7.43 | 7.07 | 6.77 | 7.17 | 7.05 | 7.33 | 8.17 | 6.67 | 6.92 | 7.13 | 6.99 | 7.44 | 8.03 | 6.84 | 7.03 | 7.06 | 7.04 |
| pH (LABORATORY) | pH (H) | 7.4 | 7.1 | 7.1 | 6.9 | 7.2 | 7.3 | 7.6 | 8.2 | 7.2 | 7.2 | 7.4 | 7.2 | 7.5 | 7.8 | 6.9 | 6.9 | 7.1 | 7.1 |
| PHENOXY ACID HERBICIDES (515.3) | µg/L | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | | ND | | ND | |
| PHOSPHORUS, DISSOLVED TOTAL | mg/L | 0.06 | 0.31 | 1.38 | 0.02 | 0.017 | 0.04 | 0.06 | ND | 0.07 | ND | 0.11 | 0.07 | 0.12 | 0.029 | 0.06 | ND | 1.4 | 0.16 |
| POTASSIUM | mg/L | 7.1 | 6.4 | 7.6 | 57 | 10 | 5.9 | 5.1 | 41 | 108 | 55 | 4.1 | 5 | 3.5 | 6.1 | 197 | 168 | 14 | 13 |
| POTASSIUM, DISSOLVED | mg/L | 8 | 7 | 7.2 | 55 | 10 | 5.5 | 4.6 | 42 | 111 | 50 | 4.3 | 4.8 | 3.6 | 6 | 196 | 167 | 12.8 | 13 |
| QC RATIO TDS/SEC | | 0.67 | 0.63 | 0.61 | 0.69 | 0.68 | 0.68 | 0.56 | 0.58 | 0.69 | 0.7 | 0.62 | 0.63 | 0.59 | 0.61 | 0.66 | 0.69 | 0.6 | 0.58 |
| REG. ORG. COMPOUNDS (EPA 525) | µg/L | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND | ND |
| SETTLABLE SOLIDS | mL/L | NA | NA | NA | | | | | NA | NA | NA | NA | NA | | | | | | |
| SILICA AS SiO ₂ , DISSOLVED | mg/L | 44 | 44 | 34 | 35 | 30 | 37 | 45 | 33 | 30 | 33 | 37 | 40 | 45 | 44 | 35 | 30 | 43 | 40 |
| SODIUM | mg/L | 77 | 140 | 79 | 6,834 | 338 | 124 | 148 | 2192 | 6106 | 5310 | 262 | 245 | 68 | 75 | 8,407 | 8,224 | 732 | 691 |
| SODIUM, DISSOLVED | mg/L | 78 | 141 | 79 | 6,540 | 342 | 119 | 135 | 2290 | 6270 | 4950 | 265 | 239 | 68 | 74 | 8,430 | 8,240 | 698 | 692 |
| SPECIFIC CONDUCTANCE (E.C) | µmhos/cm | 2758 | 1545 | 989 | 38,800 | 5,650 | 1,768 | 1045 | 12190 | 35020 | 29320 | 2036 | 1935 | 624 | 617 | 44,090 | 44,660 | 5,330 | 5,190 |
| SPECIFIC CONDUCTANCE (E.C) (FIELD) | µmhos/cm | 2859 | 1531 | 869 | 39,065 | 5,507 | 1,762 | 1113 | 15312 | 35040 | 29888 | 2004 | 1932 | 574 | 658 | 44,462 | 45,724 | 5,384 | 5,255 |
| STRONTIUM, DISSOLVED | µg/L | 1826 | 761 | 561 | 12,676 | 3,689 | 1,327 | 470 | 3536 | 8504 | 8507 | 868 | 855 | 273 | 260 | 8,148 | 8,301 | 3,064 | 1,861 |
| SULFATE | mg/L | NA | NA | NA | | | | | NA | NA | NA | NA | NA | | | | | | |
| SULFATE, DISSOLVED | mg/L | 85 | 175 | 87 | 1,882 | 176 | 61 | 32 | 541 | 1743 | 1430 | 258 | 239 | 25 | 23 | 2,286 | 2,207 | 210 | 220 |
| TEMPERATURE | °C | NA | NA | NA | | | | | NA | NA | NA | NA | NA | | | | | | |
| TEMPERATURE (FIELD) | °C | 10.6 | 16.8 | NA | 19.7 | 18.4 | 18.2 | 21.2 | 19.2 | 17.17 | 17.2 | 16.83 | 17 | 21.2 | 20.2 | 17.2 | 17.3 | 17.3 | 17.1 |
| TOTAL DISS. SOLIDS | mg/L | 1840 | 966 | 608 | 26,700 | 3,832 | 1,200 | 583 | 7100 | 24000 | 20500 | 1260 | | | | | | | |